

## CHAPTER 8

# THERMAL PROPERTIES OF FOODS

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**T**HERMAL properties of foods and beverages must be known to perform the various heat transfer calculations involved in the design of storage and refrigeration equipment and the estimation of process times for refrigerating, freezing, heating, or drying of foods and beverages. Because the thermal properties of foods and beverages strongly depend on chemical composition and temperature; and, because many food items are available, it is nearly impossible to experimentally determine and tabulate the thermal properties of foods and beverages for all possible conditions and compositions. However, composition data for foods and beverages are readily available from sources such as Holland et al. (1991) and USDA (1975). These data consist of the mass fractions of the major components found in food items. The thermal properties of food items can be predicted by using this composition data in conjunction with temperature dependent mathematical models of the thermal properties of the individual food constituents.

Thermophysical properties of foods and beverages that are often required for heat transfer calculations include density, specific heat, enthalpy, thermal conductivity, and thermal diffusivity. In addition, if the food item is a living organism, such as a fresh fruit or vegetable, it generates heat via respiration and loses moisture via transpiration. Both of these processes should be included in heat transfer calculations. This chapter summarizes prediction methods for estimating these thermophysical properties and includes examples on the use of these prediction methods. In addition, tables of measured thermophysical property data for various foods and beverages are provided.

### THERMAL PROPERTIES OF FOOD CONSTITUENTS

Constituents commonly found in food items include water, protein, fat, carbohydrate, fiber, and ash. Choi and Okos (1986) developed mathematical models for predicting the thermal properties of these food components as functions of temperature in the range of  $-40^{\circ}\text{F}$  to  $300^{\circ}\text{F}$  (see Table 1). Choi and Okos also developed models for predicting the thermal properties of water and ice (Table 2). Table 3 lists the composition of various food items, including the mass percentage of moisture, protein, fat, carbohydrate, fiber, and ash (USDA 1996)

### THERMAL PROPERTIES OF FOOD

In general, the thermophysical properties of a food or beverage are well behaved when the temperature of the food is above its initial freezing point. However, below the initial freezing point, the thermophysical properties vary greatly due to the complex processes involved during freezing.

The initial freezing point of a food is somewhat lower than the freezing point of pure water due to dissolved substances in the moisture in the food. At the initial freezing point, a portion of the water within the food crystallizes and the remaining solution becomes more concentrated. Thus, the freezing point of the unfrozen portion of the food is further reduced. The temperature continues to decrease as the separation of ice crystals increases the concentration of the solutes in solution and depresses the freezing point further. Thus, the ice and water fractions in the frozen food depend on temperature. Because the thermophysical properties of ice and water are quite different, the thermophysical properties of frozen foods vary dramatically with temperature. In addition, the thermophysical properties of the food above and below the freezing point are drastically different.

### WATER CONTENT

Because water is the predominant constituent in most foods, water content significantly influences the thermophysical properties of foods. Average values of moisture content (percent by mass) are given in Table 3. For fruits and vegetables, water content varies with the cultivar as well as with the stage of development or maturity when harvested, the growing conditions, and the amount of moisture lost after harvest. In general, the values given in Table 3 apply to mature products shortly after harvest. For fresh meat, the values of water content given in Table 3 are at the time of slaughter or after the usual aging period. For cured or processed products, the water content depends on the particular process or product.

### INITIAL FREEZING POINT

Foods and beverages do not freeze completely at a single temperature but rather they freeze over a range of temperatures. In fact, foods which are high in sugar content or foods packed in high syrup concentrations may never be completely frozen, even at typical frozen food storage temperatures. Thus, there is not a distinct freezing point for foods and beverages, but an initial freezing point at which the crystallization process begins.

The initial freezing point of a food or beverage is important not only for determining the proper storage conditions for the food item, but also for the calculation of thermophysical properties. During the storage of fresh fruits and vegetables, for example, the commodity temperature must be kept above its initial freezing point to avoid freezing damage. In addition, because there are drastic changes in the thermophysical properties of foods as they freeze, knowledge of the initial freezing point of a food item is necessary to accurately model its thermophysical properties. Experimentally determined values of the initial freezing point of foods and beverages are given in Table 3.

Table 1 Thermal Property Models for Food Components ( $-40^{\circ}\text{F} \leq t \leq 300^{\circ}\text{F}$ )

Thermal Property	Food Component	Thermal Property Model
Thermal Conductivity, Btu/(h-ft-°F)	Protein	$k = 9.0535 \times 10^{-2} + 4.1486 \times 10^{-4}t - 4.8467 \times 10^{-7}t^2$
	Fat	$k = 1.3273 \times 10^{-1} - 8.8405 \times 10^{-4}t - 3.1652 \times 10^{-8}t^2$
	Carbohydrate	$k = 1.0133 \times 10^{-1} + 4.9478 \times 10^{-4}t - 7.7238 \times 10^{-7}t^2$
	Fiber	$k = 9.2499 \times 10^{-2} + 4.3731 \times 10^{-4}t - 5.6500 \times 10^{-7}t^2$
	Ash	$k = 1.7553 \times 10^{-1} + 4.8292 \times 10^{-4}t - 5.1839 \times 10^{-7}t^2$
Thermal Diffusivity, ft <sup>2</sup> /h	Protein	$\alpha = 2.3170 \times 10^{-3} + 1.1364 \times 10^{-5}t - 1.7516 \times 10^{-8}t^2$
	Fat	$\alpha = 3.9137 \times 10^{-3} - 2.6765 \times 10^{-6}t - 4.5790 \times 10^{-10}t^2$
	Carbohydrate	$\alpha = 2.7387 \times 10^{-3} + 1.3198 \times 10^{-5}t - 2.7769 \times 10^{-8}t^2$
	Fiber	$\alpha = 2.4818 \times 10^{-3} + 1.2873 \times 10^{-5}t - 2.6553 \times 10^{-8}t^2$
	Ash	$\alpha = 4.5565 \times 10^{-3} + 8.9716 \times 10^{-6}t - 1.4644 \times 10^{-8}t^2$
Density, lb/ft <sup>3</sup>	Protein	$\rho = 8.3599 \times 10^1 - 1.7979 \times 10^{-2}t$
	Fat	$\rho = 5.8246 \times 10^1 - 1.4482 \times 10^{-2}t$
	Carbohydrate	$\rho = 1.0017 \times 10^2 - 1.0767 \times 10^{-2}t$
	Fiber	$\rho = 8.2280 \times 10^1 - 1.2690 \times 10^{-2}t$
	Ash	$\rho = 1.5162 \times 10^2 - 9.7329 \times 10^{-3}t$
Specific Heat, Btu/(lb-°F)	Protein	$c_p = 4.7442 \times 10^{-1} + 1.6661 \times 10^{-4}t - 9.6784 \times 10^{-8}t^2$
	Fat	$c_p = 4.6730 \times 10^{-1} + 2.1815 \times 10^{-4}t - 3.5391 \times 10^{-7}t^2$
	Carbohydrate	$c_p = 3.6114 \times 10^{-1} + 2.8843 \times 10^{-4}t - 4.3788 \times 10^{-7}t^2$
	Fiber	$c_p = 4.3276 \times 10^{-1} + 2.6485 \times 10^{-4}t - 3.4285 \times 10^{-7}t^2$
	Ash	$c_p = 2.5266 \times 10^{-1} + 2.6810 \times 10^{-4}t - 2.7141 \times 10^{-7}t^2$

Source: Choi and Okos (1986)

Table 2 Thermal Property Models for Water and Ice ( $-40^{\circ}\text{F} \leq t \leq 300^{\circ}\text{F}$ )

	Thermal Property	Thermal Property Model
Water	Thermal Conductivity, Btu/(h-ft-°F)	$k_w = 3.1064 \times 10^{-1} + 6.4226 \times 10^{-4}t - 1.1955 \times 10^{-6}t^2$
	Thermal Diffusivity, ft <sup>2</sup> /h	$\alpha_w = 4.6428 \times 10^{-3} + 1.5289 \times 10^{-5}t - 2.8730 \times 10^{-8}t^2$
	Density, lb/ft <sup>3</sup>	$\rho_w = 6.2174 \times 10^1 + 4.7425 \times 10^{-3}t - 7.2397 \times 10^{-5}t^2$
	Specific Heat, Btu/(lb-°F) (For temp. range of -40 to 32°F)	$c_w = 1.0725 - 5.3992 \times 10^{-3}t + 7.3361 \times 10^{-5}t^2$
	Specific Heat, Btu/(lb-°F) (For temp. range of 32 to 300°F)	$c_w = 9.9827 \times 10^{-1} - 3.7879 \times 10^{-5}t + 4.0347 \times 10^{-7}t^2$
Ice	Thermal Conductivity, Btu/(h-ft-°F)	$k_{ice} = 1.3652 - 3.1648 \times 10^{-3}t + 1.8108 \times 10^{-5}t^2$
	Thermal Diffusivity, ft <sup>2</sup> /h	$\alpha_{ice} = 5.0909 \times 10^{-2} - 2.0371 \times 10^{-4}t + 1.1366t^2 \times 10^{-6}$
	Density, lb/ft <sup>3</sup>	$\rho_{ice} = 5.7385 \times 10^1 - 4.5333 \times 10^{-3}t$
	Specific Heat, Btu/(lb-°F)	$c_{ice} = 4.6677 \times 10^{-1} + 8.0636 \times 10^{-4}t$

Source: Choi and Okos (1986)

### ICE FRACTION

To predict the thermophysical properties of frozen foods, which depend strongly on the fraction of ice within the food, the mass fraction of water that has crystallized must be determined. For temperatures below the initial freezing point, the mass fraction of water that has crystallized in a food item is a function of temperature.

In general, food items consist of water, dissolved solids and undissolved solids. During the freezing process, as some of the liquid water crystallizes, the solids dissolved in the remaining liquid water become increasingly more concentrated, thus lowering the freezing temperature. This unfrozen solution can be assumed to obey the freezing point depression equation given by Raoult's law (Pham 1987). Thus, based on Raoult's law, Chen (1985) proposed the following model for predicting the mass fraction of ice  $x_{ice}$  in a food item:

$$x_{ice} = \frac{x_s RT_o^2 (t_f - t)}{M_s L_o (t_f - 32)(t - 32)} \quad (1)$$

where

$x_s$  = mass fraction of solids in food item  
 $M_s$  = relative molecular mass of soluble solids

$R$  = universal gas constant = 1.986 Btu/lb mol-°R

$T_o$  = freezing point of water = 491.7°R

$L_o$  = latent heat of fusion of water at 491.7°R = 143.4 Btu/lb

$t_f$  = initial freezing point of food, °F

$t$  = food temperature, °F

The relative molecular mass of the soluble solids within the food item may be estimated as follows:

$$M_s = \frac{x_s RT_o^2}{-L_o(x_{w_o} - x_b)(t_f - 32)} \quad (2)$$

where  $x_{w_o}$  is the mass fraction of water in the unfrozen food item and  $x_b$  is the mass fraction of bound water in the food (Schwartzberg 1976). Bound water is that portion of the water in a food item that is bound to solids in the food, and thus is unavailable for freezing.

The mass fraction of bound water may be estimated as follows:

$$x_b = 0.4x_p \quad (3)$$

where  $x_p$  is the mass fraction of protein in the food item.

Table 3 Unfrozen Composition Data, Initial Freezing Point, and Specific Heats of Foods<sup>a</sup>

Food Item	Moisture Content, % $x_{wo}$	Protein, % $x_p$	Fat, % $x_f$	Carbohydrate, % $x_c$	Fiber, % $x_{fb}$	Ash, % $x_a$	Initial Freezing Point, °F	Specific Heat Above Freezing, Btu/lb·°F	Specific Heat Below Freezing, Btu/lb·°F
<b>Vegetables</b>									
Artichokes, Globe	84.9	3.27	0.15	10.51	5.40	1.13	29.8	0.87	0.45
Artichokes, Jerusalem	78.0	2.00	0.01	17.44	1.60	2.54	27.5	0.83	0.44
Asparagus	92.4	2.28	0.20	4.54	2.10	0.57	30.9	0.94	0.48
Beans, snap	90.3	1.82	0.12	7.14	3.40	0.66	30.7	0.94	0.47
Beans, lima	70.2	6.84	0.86	20.16	4.90	1.89	30.9	0.73	0.40
Beets	87.6	1.61	0.17	9.56	2.80	1.08	30.0	0.90	0.40
Broccoli	90.7	2.98	0.35	5.24	3.00	0.92	30.9	0.92	0.47
Brussels sprouts	86.0	3.38	0.30	8.96	3.80	1.37	30.6	0.88	0.40
Cabbage	92.2	1.44	0.27	5.43	2.30	0.71	30.4	0.94	0.47
Carrots	87.8	1.03	0.19	10.14	3.00	0.87	29.5	0.90	0.46
Cauliflower	91.9	1.98	0.21	5.20	2.50	0.71	30.6	0.93	0.47
Celeriac	88.0	1.50	0.30	9.20	1.80	1.00	30.4	0.91	0.46
Celery	94.6	0.75	0.14	3.65	1.70	0.82	31.1	0.95	0.48
Collards	90.6	1.57	0.22	7.11	3.60	0.55	30.6	0.92	0.46
Corn, sweet, yellow	76.0	3.22	1.18	19.02	2.70	0.62	30.9	0.79	0.42
Cucumbers	96.0	0.69	0.13	2.76	0.80	0.41	31.1	0.98	0.49
Eggplant	92.0	1.02	0.18	6.07	2.50	0.71	30.6	0.94	0.48
Endive	93.8	1.25	0.20	3.35	3.10	1.41	31.8	0.94	0.48
Garlic	58.6	6.36	0.50	33.07	2.10	1.50	30.6	0.79	0.42
Ginger, root	81.7	1.74	0.73	15.09	2.00	0.77	—	0.92	0.46
Horseradish	78.7	9.40	1.40	8.28	2.00	2.26	28.8	0.78	0.42
Kale	84.5	3.30	0.70	10.01	2.00	1.53	31.1	0.89	0.46
Kohlrabi	91.0	1.70	0.10	6.20	3.60	1.00	30.2	0.92	0.47
Leeks	83.0	1.50	0.30	14.15	1.80	1.05	30.7	0.95	0.46
Lettuce, iceberg	95.9	1.01	0.19	2.09	1.40	0.48	31.6	0.96	0.48
Mushrooms	91.8	2.09	0.42	4.65	1.20	0.89	30.4	0.93	0.47
Okra	89.6	2.00	0.10	7.63	3.20	0.70	28.8	0.92	0.46
Onions	89.7	1.16	0.16	8.63	1.80	0.37	30.4	0.90	0.46
Onions, dehydrated flakes	3.9	8.95	0.46	83.28	9.20	3.38	—	—	—
Parsley	87.7	2.97	0.79	6.33	3.30	2.20	30.0	0.86	0.46
Parsnips	79.5	1.20	0.30	17.99	4.90	0.98	30.4	0.84	0.46
Peas, green	78.9	5.42	0.40	14.46	5.10	0.87	30.9	0.79	0.42
Peppers, freeze dried	2.0	17.90	3.00	68.70	21.30	8.40	—	—	—
Peppers, sweet, green	92.2	0.89	0.19	6.43	1.80	0.30	30.7	0.94	0.47
Potatoes, main crop	79.0	2.07	0.10	17.98	1.60	0.89	30.9	0.87	0.44
Potatoes, sweet	72.8	1.65	0.30	24.28	3.00	0.95	29.7	0.75	0.40
Pumpkins	91.6	1.00	0.10	6.50	0.50	0.80	30.6	0.92	0.47
Radishes	94.8	0.60	0.54	3.59	1.60	0.54	30.7	0.95	0.48
Rhubarb	93.6	0.90	0.20	4.54	1.80	0.76	30.4	0.96	0.48
Rutabaga	89.7	1.20	0.20	8.13	2.50	0.81	30.0	0.91	0.47
Salsify (vegetable oyster)	77.0	3.30	0.20	18.60	3.30	0.90	30.0	0.83	0.44
Spinach	91.6	2.86	0.35	3.50	2.70	1.72	31.5	0.94	0.48
Squash, summer	94.2	0.94	0.24	4.04	1.90	0.58	31.1	0.96	0.48
Squash, winter	87.8	0.80	0.10	10.42	1.50	0.90	30.6	0.91	0.46
Tomatoes, mature green	93.0	1.20	0.20	5.10	1.10	0.50	30.9	0.95	0.48
Tomatoes, ripe	93.8	0.85	0.33	4.64	1.10	0.42	31.1	0.95	0.48
Turnip greens	91.1	1.50	0.30	5.73	3.20	1.40	31.6	0.94	0.47
Turnip	91.9	0.90	0.10	6.23	1.80	0.70	30.0	0.93	0.47
Watercress	95.1	2.30	0.10	1.29	1.50	1.20	31.5	0.96	0.48
Yams	69.6	1.53	0.17	27.89	4.10	0.82	—	0.84	0.42
<b>Fruits</b>									
Apples, fresh	83.9	0.19	0.36	15.25	2.70	0.26	30.0	0.86	0.44
Apples, dried	31.8	0.93	0.32	65.89	8.70	1.10	—	0.54	0.27
Apricots	86.3	1.40	0.39	11.12	2.40	0.75	30.0	0.88	0.46
Avocados	74.3	1.98	15.32	7.39	5.00	1.04	31.5	0.91	0.49
Bananas	74.3	1.03	0.48	23.43	2.40	0.80	30.6	0.80	0.42

Table 3 Unfrozen Composition Data, Initial Freezing Point, and Specific Heats of Foods<sup>a</sup> (Continued)

Food Item	Moisture	Protein,	Fat,	Carbohydrate,	Fiber,	Ash,	Initial	Specific Heat	Specific Heat
	Content, %	%	%	%	%	%	Freezing Point, °F	Above Freezing, Btu/lb·°F	Below Freezing Btu/lb·°F
	$x_{wo}$	$x_p$	$x_f$	$x_c$	$x_{fb}$	$x_a$			
Blackberries	85.6	0.72	0.39	12.76	5.30	0.48	30.6	0.88	0.40
Blueberries	84.6	0.67	0.38	14.13	2.70	0.21	29.1	0.86	0.45
Cantaloupes	89.8	0.88	0.28	8.36	0.80	0.71	29.8	0.94	0.48
Cherries, sour	86.1	1.00	0.30	12.18	1.60	0.40	28.9	0.87	0.45
Cherries, sweet	80.8	1.20	0.96	16.55	2.30	0.53	28.8	0.87	0.45
Cranberries	86.5	0.39	0.20	12.68	4.20	0.19	30.4	0.90	0.46
Currants, European black	82.0	1.40	0.41	15.38	0.00	0.86	30.2	0.91	0.46
Currants, red and white	84.0	1.40	0.20	13.80	4.30	0.66	30.2	0.91	0.46
Dates, cured	22.5	1.97	0.45	73.51	7.50	1.58	3.7	0.36	0.26
Figs, fresh	79.1	0.75	0.30	19.18	3.30	0.66	27.7	0.82	0.43
Figs, dried	28.4	3.05	1.17	65.35	9.30	2.01	—	0.39	0.27
Gooseberries	87.9	0.88	0.58	10.18	4.30	0.49	30.0	0.90	0.46
Grapefruit	90.9	0.63	0.10	8.08	1.10	0.31	30.0	0.91	0.46
Grapes, American	81.3	0.63	0.35	17.15	1.00	0.57	29.1	0.86	0.44
Grapes, European type	80.6	0.66	0.58	17.77	1.00	0.44	28.2	0.86	0.44
Lemons	87.4	1.20	0.30	10.70	4.70	0.40	29.5	0.92	0.46
Limes	88.3	0.70	0.20	10.54	2.80	0.30	29.1	0.89	0.46
Mangos	81.7	0.51	0.27	17.00	1.80	0.50	30.4	0.90	0.46
Melons, casaba	92.0	0.90	0.10	6.20	0.80	0.80	30.0	0.96	0.48
Melons, honeydew	89.7	0.46	0.10	9.18	0.60	0.60	30.4	0.94	0.48
Melons, watermelon	91.5	0.62	0.43	7.18	0.50	0.26	31.3	0.97	0.48
Nectarines	86.3	0.94	0.46	11.78	1.60	0.54	30.4	0.90	0.49
Olives	80.0	0.84	10.68	6.26	3.20	2.23	29.5	0.80	0.42
Oranges	82.3	1.30	0.30	15.50	4.50	0.60	30.6	0.90	0.46
Peaches, fresh	87.7	0.70	0.90	11.10	2.00	0.46	30.4	0.90	0.46
Peaches, dried	31.8	3.61	0.76	61.33	8.20	2.50	—	0.55	0.28
Pears	83.8	0.39	0.40	15.11	2.40	0.28	29.1	0.90	0.45
Persimmons	64.4	0.80	0.40	33.50	0.00	0.90	28.0	0.84	0.43
Pineapples	86.5	0.39	0.43	12.39	1.20	0.29	30.2	0.88	0.45
Plums	85.2	0.79	0.62	13.01	1.50	0.39	30.6	0.84	0.46
Pomegranates	81.0	0.95	0.30	17.17	0.60	0.61	26.6	0.88	0.48
Prunes, dried	32.4	2.61	0.52	62.73	7.10	1.76	—	0.57	0.28
Quinces	83.8	0.40	0.10	15.30	1.90	0.40	28.4	0.88	0.45
Raisins, seedless	15.4	3.22	0.46	79.13	4.00	1.77	—	0.47	0.26
Raspberries	86.6	0.91	0.55	11.57	6.80	0.40	30.9	0.85	0.45
Strawberries	91.6	0.61	0.37	7.02	2.30	0.43	30.6	0.93	0.27
Tangerines	87.6	0.63	0.19	11.19	2.30	0.39	30.0	0.93	0.50
<b>Whole Fish</b>									
Cod	81.2	17.81	0.67	0.0	0.0	1.16	28.0	0.90	0.49
Haddock	79.9	18.91	0.72	0.0	0.0	1.21	28.0	0.82	0.43
Halibut	77.9	20.81	2.29	0.0	0.0	1.36	28.0	0.80	0.43
Herring, kippered	59.7	24.58	12.37	0.0	0.0	1.94	28.0	0.76	0.41
Mackerel, Atlantic	63.6	18.60	13.89	0.0	0.0	1.35	28.0	0.66	0.37
Perch	78.7	18.62	1.63	0.0	0.0	1.20	28.0	0.84	0.44
Pollock, Atlantic	78.2	19.44	0.98	0.0	0.0	1.41	28.0	0.83	0.44
Salmon, pink	76.4	19.94	3.45	0.0	0.0	1.22	28.0	0.71	0.39
Tuna, bluefin	68.1	23.33	4.90	0.0	0.0	1.18	28.0	0.76	0.41
Whiting	80.3	18.31	1.31	0.0	0.0	1.30	28.0	0.86	0.44
<b>Shellfish</b>									
Clams	81.8	12.77	0.97	2.57	0.0	1.87	28.0	—	—
Lobster, American	76.8	18.80	0.90	0.50	0.0	2.20	28.0	0.83	0.44
Oysters	85.2	7.05	2.46	3.91	0.0	1.42	28.0	0.83	0.44
Scallop, meat	78.6	16.78	0.76	2.36	0.0	1.53	28.0	0.84	0.44
Shrimp	75.9	20.31	1.73	0.91	0.0	1.20	28.0	0.83	0.45
<b>Beef</b>									
Brisket	55.2	16.94	26.54	0.0	0.0	0.80	—	—	—
Carcass, choice	57.3	17.32	24.05	0.0	0.0	0.81	28.0	—	—
Carcass, select	58.2	17.48	22.55	0.0	0.0	0.82	28.9	—	—

Table 3 Unfrozen Composition Data, Initial Freezing Point, and Specific Heats of Foods<sup>a</sup> (Continued)

Food Item	Moisture Content, % $x_{wo}$	Protein, % $x_p$	Fat, % $x_f$	Carbohydrate, % $x_c$	Fiber, % $x_{fb}$	Ash, % $x_a$	Initial Freezing Point, °F	Specific Heat Above Freezing, Btu/lb·°F	Specific Heat Below Freezing, Btu/lb·°F
Liver	69.0	20.00	3.85	5.82	0.0	1.34	28.9	0.82	0.41
Ribs, whole (ribs 6-12)	54.5	16.37	26.98	0.0	0.0	0.77	—	—	—
Round, full cut, lean and fat	64.8	20.37	12.81	0.0	0.0	0.97	—	0.80	0.40
Round, full cut, lean	70.8	22.03	4.89	0.0	0.0	1.07	—	0.80	0.40
Sirloin, lean	71.7	21.24	4.40	0.0	0.0	1.08	28.9	0.74	0.37
Short loin, porterhouse steak, lean	69.6	20.27	8.17	0.0	0.0	1.01	—	—	—
Short loin, T-Bone steak, lean	69.7	20.78	7.27	0.0	0.0	1.27	—	—	—
Tenderloin, lean	68.4	20.78	7.90	0.0	0.0	1.04	—	—	—
Veal, lean	75.9	20.20	2.87	0.0	0.0	1.08	—	0.80	0.46
<b>Pork</b>									
Fatback	7.7	2.92	88.69	0.0	0.0	0.70	—	0.62	0.23
Bacon	31.6	8.66	57.54	0.09	0.0	2.13	—	0.50	0.30
Belly	36.7	9.34	53.01	0.0	0.0	0.49	—	0.58	0.29
Carcass	49.8	13.91	35.07	0.0	0.0	0.72	—	0.62	0.31
Ham, cured, whole lean	68.3	22.32	5.71	0.05	0.0	3.66	—	0.74	0.37
Ham, country cured lean	55.9	27.80	8.32	0.30	0.0	7.65	—	0.65	0.33
Shoulder, whole, lean	72.6	19.55	7.14	0.0	0.0	1.02	28.0	0.69	0.35
<b>Sausage</b>									
Braunschweiger	48.0	13.50	32.09	3.13	0.0	3.27	—	—	—
Frankfurter	53.9	11.28	29.15	2.55	0.0	3.15	28.9	0.86	0.56
Italian	51.1	14.25	31.33	0.65	0.0	2.70	—	—	—
Polish	53.2	14.10	28.72	1.63	0.0	2.40	—	0.72	0.36
Pork	44.5	11.69	40.29	1.02	0.0	2.49	—	0.89	0.56
Smoked links	39.3	22.20	31.70	2.10	0.0	4.70	—	0.86	0.56
<b>Poultry Products</b>									
Chicken	66.0	18.60	15.06	0.0	0.0	0.79	27.0	0.79	0.37
Duck	48.5	11.49	39.34	0.0	0.0	0.68	—	0.81	0.41
Turkey	70.4	20.42	8.02	0.0	0.0	0.88	—	0.79	0.37
<b>Egg</b>									
White	87.8	10.52	0.0	1.03	0.0	0.64	30.9	0.93	0.47
White, dried	14.6	76.92	0.04	4.17	0.0	4.25	—	0.45	0.23
Whole	75.3	12.49	10.02	1.22	0.0	0.94	30.9	0.76	0.40
Whole, dried	3.1	47.35	40.95	4.95	0.0	3.65	—	0.25	0.21
Yolk	48.8	16.76	30.87	1.78	0.0	1.77	30.9	0.67	0.35
Yolk, salted	50.8	14.00	23.00	1.60	0.0	10.60	1.0	0.70	0.35
Yolk, sugared	51.2	13.80	22.75	10.80	0.0	1.40	25.0	0.71	0.35
<b>Lamb</b>									
Composite of cuts, lean	73.4	20.29	5.25	0.0	0.0	1.06	28.6	0.77	0.39
Leg, whole, lean	74.1	20.56	4.51	0.0	0.0	1.07	—	0.79	0.40
<b>Dairy Products</b>									
Butter	17.9	0.85	81.11	0.06	0.0	0.04	—	0.52	—
<b>Cheese</b>									
Camembert	51.8	19.80	24.26	0.46	0.0	3.68	—	0.71	0.36
Cheddar	36.8	24.90	33.14	1.28	0.0	3.93	8.8	0.62	0.31
Cottage, uncreamed	79.8	17.27	0.42	1.85	0.0	0.69	29.8	0.87	0.44
Cream	53.8	7.55	34.87	2.66	0.0	1.17	—	0.70	0.45
Gouda	41.5	24.94	27.44	2.22	0.0	3.94	—	—	—
Limburger	48.4	20.05	27.25	0.49	0.0	3.79	18.7	0.70	0.40
Mozzarella	54.1	19.42	21.60	2.22	0.0	2.62	—	—	—
Parmesan, hard	29.2	35.75	25.83	3.22	0.0	6.04	—	—	—
Roquefort	39.4	21.54	30.64	2.00	0.0	6.44	2.7	0.65	0.32
Swiss	37.2	28.43	27.45	3.38	0.0	3.53	14.0	0.64	0.36
Processed American	39.2	22.15	31.25	1.30	0.0	5.84	19.6	0.64	0.32
<b>Cream</b>									
Half and half	80.6	2.96	11.50	4.30	0.0	0.67	—	0.88	0.44
Table	73.8	2.70	19.31	3.66	0.0	0.58	28.0	0.83	0.42
Heavy whipping	57.7	2.05	37.00	2.79	0.0	0.45	—	0.85	0.40

Table 3 Unfrozen Composition Data, Initial Freezing Point, and Specific Heats of Foods<sup>a</sup> (Continued)

Food Item	Moisture Content, % $x_{wo}$	Protein, % $x_p$	Fat, % $x_f$	Carbohydrate, % $x_c$	Fiber, % $x_{fb}$	Ash, % $x_a$	Initial Freezing Point, °F	Specific Heat Above Freezing, Btu/lb·°F	Specific Heat Below Freezing Btu/lb·°F
<b>Ice Cream</b>									
Chocolate	55.7	3.80	11.0	28.20	1.20	1.00	21.9	0.78	0.45
Strawberry	60.0	3.20	8.40	27.60	0.30	0.70	21.9	0.78	0.45
Vanilla	61.0	3.50	11.00	23.60	0.0	0.90	21.9	0.78	0.45
<b>Milk</b>									
Canned, condensed sweetened	27.2	7.91	8.70	54.40	0.0	1.83	5.0	0.56	0.28
Evaporated	74.0	6.81	7.56	10.04	0.0	1.55	29.5	0.84	0.42
Skim	90.8	3.41	0.18	4.85	0.0	0.76	—	0.96	0.60
Skim, dried	3.2	36.16	0.77	51.98	0.0	7.93	—	0.42	0.21
Whole	87.7	3.28	3.66	4.65	0.0	0.72	30.9	0.92	0.46
Whole, dried	2.5	26.32	26.71	38.42	0.0	6.08	—	0.41	0.21
Whey, acid, dried	3.5	11.73	0.54	73.45	0.0	10.77	—	0.43	0.22
Whey, sweet, dried	3.2	12.93	1.07	74.46	0.0	8.35	—	0.43	0.22
<b>Nuts, Shelled</b>									
Almonds	4.4	19.95	52.21	20.40	10.90	3.03	—	0.43	0.22
Filberts	5.4	13.04	62.64	15.30	6.10	3.61	—	0.44	0.22
Peanuts, raw	6.5	25.80	49.24	16.14	8.50	2.33	—	0.44	0.22
Peanuts, dry roasted with salt	1.6	23.68	49.66	21.51	8.00	3.60	—	0.41	0.21
Pecans	4.8	7.75	67.64	18.24	7.60	1.56	—	0.42	0.21
Walnuts, English	3.6	14.29	61.87	18.34	4.80	1.86	—	0.43	0.21
<b>Candy</b>									
Fudge, vanilla	10.9	1.10	5.40	82.30	0.0	0.40	—	0.46	0.23
Marshmallows	16.4	1.80	0.20	81.30	0.10	0.30	—	0.50	0.25
Milk chocolate	1.3	6.90	30.70	59.20	3.40	1.50	—	0.41	0.20
Peanut brittle	1.8	7.50	19.10	69.30	2.00	1.50	—	0.41	0.21
<b>Juice and Beverages</b>									
Apple juice, unsweetened	87.9	0.06	0.11	11.68	0.10	0.22	—	0.91	0.47
Grapefruit juice, sweetened	87.4	0.58	0.09	11.13	0.10	0.82	—	0.90	0.46
Grape juice, unsweetened	84.1	0.56	0.08	14.96	0.10	0.29	—	0.88	0.45
Lemon juice	92.5	0.40	0.29	6.48	0.40	0.36	—	0.94	0.48
Lime juice, unsweetened	92.5	0.25	0.23	6.69	0.40	0.31	—	0.94	0.48
Orange juice	89.0	0.59	0.14	9.85	0.20	0.41	31.3	0.91	0.47
Pineapple juice, unsweetened	85.5	0.32	0.08	13.78	0.20	0.30	—	0.89	0.46
Prune juice	81.2	0.61	0.03	17.45	1.00	0.68	—	0.85	0.45
Tomato juice	93.9	0.76	0.06	4.23	0.40	1.05	—	0.95	0.48
Cranberry-apple juice drink	82.8	0.10	0.0	17.10	0.10	0.0	—	0.86	0.45
Cranberry-grape juice drink	85.6	0.20	0.10	14.00	0.10	0.10	—	0.89	0.46
Fruit punch drink	88.0	0.0	0.0	11.90	0.10	0.10	—	0.91	0.47
Club soda	99.9	0.0	0.0	0.0	0.0	0.10	—	1.00	0.50
Cola	89.4	0.0	0.0	10.40	0.0	0.10	—	0.92	0.47
Cream soda	86.7	0.0	0.0	13.30	0.0	0.10	—	0.89	0.46
Ginger ale	91.2	0.0	0.0	8.70	0.0	0.0	—	0.93	0.48
Grape soda	88.8	0.0	0.0	11.20	0.0	0.10	—	0.91	0.47
Lemon-lime soda	89.5	0.0	0.0	10.40	0.0	0.10	—	0.92	0.47
Orange soda	87.6	0.0	0.0	12.30	0.0	0.10	—	0.90	0.46
Root beer	89.3	0.0	0.0	10.60	0.0	0.10	—	0.92	0.47
Chocolate milk, 2% fat	83.6	3.21	2.00	10.40	0.50	0.81	—	0.87	0.45
<b>Miscellaneous</b>									
Honey	17.1	0.30	0.0	82.40	0.20	0.20	—	—	—
Maple syrup	32.0	0.00	0.20	67.20	0.0	0.60	—	0.49	0.31
Popcorn, air-popped	4.1	12.00	4.20	77.90	15.10	1.80	—	—	—
Popcorn, oil-popped	2.8	9.00	28.10	57.20	10.00	2.90	—	—	—
Yeast, baker's, compressed	69.0	8.40	1.90	18.10	8.10	1.80	—	0.77	0.41

<sup>a</sup>Composition data from USDA (1996). Initial freezing point data from ASHRAE (1993). Specific heats from Polley et al. (1980) and ASHRAE (1993).

Substitution of Equation (2) for relative molecular mass into Equation (1) yields a simple method for predicting the ice fraction as follows (Miles 1974):

$$x_{ice} = (x_{wo} - x_b) \left[ 1 - \frac{t_f - 32}{t - 32} \right] \quad (4)$$

Because Equation (4) underestimates the ice fraction at temperatures near the initial freezing point and overestimates the ice fraction at lower temperatures, Tchigeov (1979) proposed an empirical relationship to estimate the mass fraction of ice:

$$x_{ice} = \frac{1.105x_{wo}}{1 + \frac{0.7138}{\ln[1 + (t_f - t)/1.8]}} \quad (5)$$

Fikiin (1996) notes that Equation (5) applies to a wide variety of food items and provides satisfactory accuracy.

**Example 1.** A 300 lb beef carcass is to be frozen to a temperature of 0°F. What is the mass of the frozen water and the mass of the unfrozen water at 0°F?

**Solution:**

From Table 3, the mass fraction of water in the beef carcass is 0.58 and the initial freezing point for the beef carcass is 28.9°F. Using Equation (5), the mass fraction of ice is:

$$x_{ice} = \frac{1.105 \times 0.58}{1 + \frac{0.7138}{\ln[1 + (28.9 - 0)/1.8]}} = 0.51$$

The mass fraction of unfrozen water is:

$$x_u = x_{wo} - x_{ice} = 0.58 - 0.51 = 0.07$$

The mass of frozen water at 0°F is:

$$x_{ice} \times 300 \text{ lb} = 0.51 \times 300 = 153 \text{ lb}$$

The mass of unfrozen water at 0°F is:

$$x_u \times 300 \text{ lb} = 0.07 \times 300 = 21 \text{ lb}$$

### DENSITY

Modeling the density of foods and beverages requires knowledge of the food porosity, as well as the mass fraction and density of the food components. The density  $\rho$  of foods and beverages can be calculated accordingly:

$$\rho = \frac{(1 - \epsilon)}{\sum x_i / \rho_i} \quad (6)$$

where  $\epsilon$  is the porosity,  $x_i$  is the mass fraction of the food constituents, and  $\rho_i$  is the density of the food constituents. The porosity  $\epsilon$  is required to model the density of granular food items stored in bulk, such as grains and rice. For other food items, the porosity is zero.

### SPECIFIC HEAT

Specific heat is a measure of the energy required to change the temperature of a food item by one degree. Therefore, the specific heat of foods or beverages can be used to calculate the heat load imposed on the refrigeration equipment by the cooling or freezing of foods and beverages. In unfrozen foods, specific heat becomes slightly lower as the temperature rises from 32°F to 68°F. For frozen foods, there is a large decrease in specific heat as the temperature decreases. Table 3 lists experimentally determined values of the specific heats for various foods above and below freezing.

### Unfrozen Food

The specific heat of a food item, at temperatures above its initial freezing point, can be obtained from the mass average of the specific heats of the food components. Thus, the specific heat of an unfrozen food item  $c_u$  may be determined as follows:

$$c_u = \sum c_i x_i \quad (7)$$

where  $c_i$  is the specific heat of the individual food components and  $x_i$  is the mass fraction of the food components.

A simpler model for the specific heat of an unfrozen food item is presented by Chen (1985). If detailed composition data is not available, the following expression for the specific heat of an unfrozen food item can be used:

$$c_u = 1.0 - 0.55x_s - 0.15x_s^3 \quad (8)$$

where  $c_u$  is the specific heat of the unfrozen food item in Btu/lb·°F and  $x_s$  is the mass fraction of the solids in the food item.

### Frozen

Below the freezing point of the food item, the sensible heat due to temperature change and the latent heat due to the fusion of water must be considered. Because latent heat is not released at a constant temperature, but rather over a range of temperatures, an apparent specific heat must be used to account for both the sensible and latent heat effects. A common method to predict the apparent specific heat of food items is that of Schwartzberg (1976):

$$c_a = c_u + (x_b - x_{wo})\Delta c + Ex_s \left[ \frac{RT_o^2}{M_w(t - 32)^2} - 0.8\Delta c \right] \quad (9)$$

where

- $c_a$  = apparent specific heat
- $c_u$  = specific heat of food item above initial freezing point
- $x_b$  = mass fraction of bound water
- $x_{wo}$  = mass fraction of water above initial freezing point
- $\Delta c$  = difference between specific heats of water and ice =  $c_w - c_{ice}$
- $E$  = ratio of relative molecular masses of water  $M_w$  and food solids  $M_s$  ( $E = M_w/M_s$ )
- $R$  = universal gas constant = 1.986 Btu/lb mol·°R
- $T_o$  = freezing point of water = 491.7°R
- $t$  = food temperature

The specific heat of the food item above the freezing point may be estimated with Equation (7) or Equation (8).

Schwartzberg (1981) expanded on his earlier work and developed an alternative method for determining the apparent specific heat of a food item below the initial freezing point as follows:

$$c_a = c_f + (x_{wo} - x_b) \left[ \frac{L_o(t_o - t_f)}{t_o - t} \right] \quad (10)$$

where

- $c_f$  = specific heat of fully frozen food item (typically at -40°F)
- $t_o$  = freezing point of water = 32°F
- $t_f$  = initial freezing point of food, °F
- $t$  = food temperature, °F
- $L_o$  = latent heat of fusion of water = 143.4 Btu/lb

Experimentally determined values of the specific heat of fully frozen food items are given in Table 3.

A slightly simpler apparent specific heat model, which is similar in form to that of Schwartzberg (1976), was developed by Chen

(1985). Chen's model is an expansion of Siebel's equation (Siebel 1892) for specific heat and has the following form:

$$c_a = 0.37 + 0.30x_s + \frac{x_s RT_o^2}{M_s(t-32)^2} \quad (11)$$

where

- $c_a$  = apparent specific heat, Btu/lb·°F
- $x_s$  = mass fraction of solids
- $R$  = universal gas constant
- $T_o$  = freezing point of water = 491.7°R
- $M_s$  = relative molecular mass of soluble solids in food item
- $t$  = food temperature, °F

If the relative molecular mass of the soluble solids is unknown, Equation (2) may be used to estimate the molecular mass. Substitution of Equation (2) into Equation (11) yields:

$$c_a = 0.37 + 0.30x_s - \frac{L_o(x_{wo} - x_b)(t_f - 32)}{(t - 32)^2} \quad (12)$$

**Example 2.** A 300 lb lamb is to be cooled from 50°F to 32°F. Using the specific heat, determine the amount of heat which must be removed from the lamb.

**Solution:**

From Table 3, the composition of lamb is given as follows:

$$\begin{array}{ll} x_{wo} = 0.7342 & x_f = 0.0525 \\ x_p = 0.2029 & x_a = 0.0106 \end{array}$$

Evaluate the specific heat of lamb at an average temperature of  $(50 + 32)/2 = 41^\circ\text{F}$ . From Tables 1 and 2, the specific heat of the food constituents may be determined as follows:

$$c_w = 9.9827 \times 10^{-1} - 3.7879 \times 10^{-5}(41) + 4.0347 \times 10^{-7}(41)^2 = 0.9974 \text{ Btu/lb}\cdot^\circ\text{F}$$

$$c_p = 4.7442 \times 10^{-1} + 1.6661 \times 10^{-4}(41) - 9.6784 \times 10^{-8}(41)^2 = 0.4811 \text{ Btu/lb}\cdot^\circ\text{F}$$

$$c_f = 4.6730 \times 10^{-1} + 2.1815 \times 10^{-4}(41) - 3.5391 \times 10^{-7}(41)^2 = 0.4756 \text{ Btu/lb}\cdot^\circ\text{F}$$

$$c_a = 2.5266 \times 10^{-1} + 2.6810 \times 10^{-4}(41) - 2.7141 \times 10^{-7}(41)^2 = 0.2632 \text{ Btu/lb}\cdot^\circ\text{F}$$

The specific heat of lamb can be calculated with Equation (7):

$$c = \sum c_i x_i = (0.9974)(0.7342) + (0.4811)(0.2029) + (0.4756)(0.0525) + (0.2632)(0.0106)$$

$$c = 0.858 \text{ Btu/lb}\cdot^\circ\text{F}$$

The heat to be removed from the lamb is as follows:

$$Q = mc\Delta T = 300 \times 0.858 (50 - 32) = 4630 \text{ Btu}$$

## ENTHALPY

The change in enthalpy of a food item can be used to estimate the energy that must be added or removed to effect a temperature change. Above the freezing point, enthalpy consists of sensible energy, while below the freezing point, enthalpy consists of both sensible and latent energy. Enthalpy may be obtained from the definition of constant pressure specific heat:

$$c_p = \left( \frac{\partial H}{\partial T} \right)_p \quad (13)$$

where  $c_p$  is constant pressure specific heat,  $H$  is enthalpy, and  $T$  is temperature. Mathematical models for enthalpy may be obtained by integrating expressions of specific heat with respect to temperature.

## Unfrozen Food

For food items that are at temperatures above their initial freezing point, enthalpy may be obtained by integrating the corresponding expression for specific heat above the freezing point. Thus, the enthalpy of an unfrozen food item  $H$  may be determined by integrating Equation (7) as follows:

$$H = \sum H_i x_i = \sum \int c_i x_i dT \quad (14)$$

where  $H_i$  is the enthalpy of the individual food components and  $x_i$  is the mass fraction of the food components.

In the case of the method of Chen (1985), the enthalpy of an unfrozen food may be obtained by integrating Equation (8):

$$H = H_f + (t - t_f)(1.0 - 0.55x_s - 0.15x_s^3) \quad (15)$$

where

- $H$  = enthalpy of food item, Btu/lb
- $H_f$  = enthalpy of food at initial freezing temperature, Btu/lb
- $t$  = temperature of food item, °F
- $t_f$  = initial freezing temperature of food item, °F
- $x_s$  = mass fraction of food solids

The enthalpy at the initial freezing point  $H_f$  may be estimated by evaluating either Equation (17) or (18) at the initial freezing temperature of the food as discussed in the following section.

## Frozen Foods

For food items below the initial freezing point, mathematical expressions for enthalpy may be obtained by integrating the previously mentioned apparent specific heat models. Integration of Equation (9) between a reference temperature  $T_r$  and the food temperature  $T$  leads to the following expression for the enthalpy of a food item (Schwartzberg 1976):

$$H = (T - T_r) \times \left\{ c_u + (x_b - x_{wo})\Delta c + E x_s \left[ \frac{RT_o^2}{18(T_o - T_r)(T_o - T)} - 0.8\Delta c \right] \right\} \quad (16)$$

Generally, the reference temperature  $T_r$  is taken to be 419.7°R (−40°F) at which point the enthalpy is defined to be zero.

By integrating Equation (11) between a reference temperature  $T_r$  and the food temperature  $T$ , Chen (1985) obtained the following expression for enthalpy below the initial freezing point:

$$H = (t - t_r) \left( 0.37 + 0.30x_s + \frac{x_s RT_o^2}{M_s(t-32)(t_r-32)} \right) \quad (17)$$

where

- $H$  = enthalpy of food item
- $R$  = universal gas constant
- $T_o$  = freezing point of water = 491.7°R

Substitution of Equation (2) for the relative molecular mass of the soluble solids  $M_s$  simplifies Chen's method as follows:

$$H = (t - t_r) \left[ 0.37 + 0.30x_s - \frac{(x_{wo} - x_b)L_o(t_f - 32)}{(t_r - 32)(t - 32)} \right] \quad (18)$$

As an alternative to the enthalpy models developed by integration of specific heat equations, Chang and Tao (1981) developed empirical correlations for the enthalpy of food items. Their enthalpy correlations are given as functions of water content, initial and final



temperatures, and food type (meat, juice or fruit/vegetable). The correlations at a reference temperature of  $(-50^\circ\text{F})$  have the following form:

$$H = H_f(y\bar{T} + (1 - y)\bar{T}^z) \quad (19)$$

where

- $H$  = enthalpy of food item, Btu/lb
- $H_f$  = enthalpy of food item at initial freezing temperature, Btu/lb
- $\bar{T}$  = reduced temperature,  $\bar{T} = (T - T_r)/(T_f - T_r)$
- $T_r$  = reference temperature (zero enthalpy) =  $409.7^\circ\text{R}$  ( $-50^\circ\text{F}$ )
- $y, z$  = correlation parameters

By performing regression analysis on experimental data available in the literature, Chang and Tao (1981) developed the following correlation parameters  $y$  and  $z$  used in Equation (19):

**Meat Group:**

$$y = 0.316 - 0.247(x_{wo} - 0.73) - 0.688(x_{wo} - 0.73)^2$$

$$z = 22.95 - 54.68(y - 0.28) - 5589.03(y - 0.28)^2 \quad (20)$$

**Fruit, Vegetable, and Juice Group:**

$$y = 0.362 + 0.0498(x_{wo} - 0.73) - 3.465(x_{wo} - 0.73)^2$$

$$z = 27.2 - 129.04(y - 0.23) - 481.46(y - 0.23)^2 \quad (21)$$

They also developed correlations to estimate the initial freezing temperature  $T_f$  for use in Equation (19). These correlations give  $T_f$  as a function of water content:

**Meat Group:**

$$T_f = 488.12 + 2.65x_{wo} \quad (22)$$

**Fruit/Vegetable Group:**

$$T_f = 517.61 - 88.54x_{wo} + 66.73x_{wo}^2 \quad (23)$$

**Juice Group:**

$$T_f = 216.85 + 589.23x_{wo} - 317.68x_{wo}^2 \quad (24)$$

In addition, the enthalpy of the food item at its initial freezing point is required in Equation (19). Chang and Tao (1981) suggest the following correlation for determining the enthalpy of the food item at its initial freezing point  $H_f$

$$H_f = 4.21 + 0.17416x_{wo} \quad (25)$$

Table 4 presents experimentally determined values for the enthalpy of some frozen foods at a reference temperature of  $-40^\circ\text{F}$  as well as the percentage of unfrozen water in these foods.

**Example 3.** A 300 lb beef carcass is to be frozen to a temperature of  $0^\circ\text{F}$ . The initial temperature of the beef carcass is  $50^\circ\text{F}$ . How much heat must be removed from the beef carcass during this process?

**Solution:**

From Table 3, the mass fraction of water in the beef carcass is 0.5821, the mass fraction of protein in the beef carcass is 0.1748 and the initial freezing point of the beef carcass is  $28.9^\circ\text{F}$ . The mass fraction of solids in the beef carcass is:

$$x_s = 1 - x_{wo} = 1 - 0.5821 = 0.4179$$

The mass fraction of bound water is given by Equation (3):

$$x_b = 0.4x_p = 0.4 \times 0.1748 = 0.0699$$

The enthalpy of the beef carcass at  $0^\circ\text{F}$  is given by Equation (18) for frozen foods:

$$H_0 = [0 - (-40)] \left\{ 0.37 + 0.30 \times 0.4179 - \frac{(0.5821 - 0.0699)143.4(28.9 - 32)}{(-40 - 32)(0 - 32)} \right\} = 23.77 \text{ Btu/lb}$$

The enthalpy of the beef carcass at the initial freezing point is determined by evaluating Equation (18) at the initial freezing point:

$$H_f = [28.9 - (-40)] \left\{ 0.37 + 0.30 \times 0.4179 - \frac{(0.5821 - 0.0699)143.4(28.9 - 32)}{(-40 - 32)(28.9 - 32)} \right\} = 104.42 \text{ Btu/lb}$$

The enthalpy of the beef carcass at  $50^\circ\text{F}$  is given by Equation (15) for unfrozen foods:

$$H_{50} = 104.42 + (50 - 28.9) \times [1 - 0.55(0.4179) - 0.15(0.4179)^3] = 120.44 \text{ Btu/lb}$$

Thus, the amount of heat removed during the freezing process is:

$$Q = m\Delta H = m(H_{50} - H_0) = 300(120.44 - 23.77) = 29,000 \text{ Btu}$$

**THERMAL CONDUCTIVITY**

Thermal conductivity relates the conduction heat transfer rate to the temperature gradient. The thermal conductivity of a food depends on such factors as composition, structure, and temperature. Early work in the modeling of thermal conductivity of foods and beverages includes Eucken's adaption of Maxwell's equation (Eucken 1940). This model is based on the thermal conductivity of dilute dispersions of small spheres in a continuous phase:

$$k = k_c \frac{1 - [1 - a(k_d/k_c)]b}{1 + (a - 1)b} \quad (26)$$

where

- $k$  = conductivity of mixture
- $k_c$  = conductivity of continuous phase
- $k_d$  = conductivity of dispersed phase
- $a = 3k_c/(2k_c + k_d)$
- $b = V_d/(V_c + V_d)$
- $V_d$  = volume of dispersed phase
- $V_c$  = volume of continuous phase

In an effort to account for the different structural features of foods, Kopelman (1966) developed thermal conductivity models for homogeneous and fibrous food items. The differences in thermal conductivity parallel and perpendicular to the food fibers are accounted for in Kopelman's fibrous food thermal conductivity models.

For an isotropic, two-component system composed of continuous and discontinuous phases, in which the thermal conductivity is independent of the direction of heat flow, Kopelman (1966) developed the following expression for thermal conductivity  $k$ :

$$k = k_c \left[ \frac{1 - L^2}{1 - L^2(1 - L)} \right] \quad (27)$$

**Table 4 Enthalpy of Frozen Foods**

Product	Water Content, % (mass)		Temperature, °F															
			-40	-20	-10	-5	0	5	10	15	18	20	22	24	26	28	30	32
<b>Fruits and Vegetables</b>																		
Applesauce	82.8	Enthalpy, Btu/lb	0	11	17	21	25	30	36	43	49	56	61	71	84	114	145	147
		% water unfrozen	—	5	7	9	11	14	17	20	25	28	33	41	52	76	100	—
Asparagus, peeled	92.6	Enthalpy, Btu/lb	0	8	14	16	19	22	26	30	34	37	40	44	51	63	101	162
		% water unfrozen	—	—	—	4	5	6	7	9	10	12	16	20	28	55	100	—
Bilberries	85.1	Enthalpy, Btu/lb	0	10	15	18	22	25	30	37	41	45	50	56	67	87	149	151
		% water unfrozen	—	—	5	6	7	9	11	14	17	19	22	27	35	50	100	—
Carrots	87.5	Enthalpy, Btu/lb	0	10	15	18	22	26	31	37	41	45	50	57	68	88	152	154
		% water unfrozen	—	—	5	6	7	9	11	14	17	19	22	27	35	50	100	—
Cucumbers	95.4	Enthalpy, Btu/lb	0	8	13	16	18	21	24	27	30	32	35	38	43	52	78	167
		% water unfrozen	—	—	—	—	—	—	—	—	6	7	8	9	12	18	36	100
Onions	85.5	Enthalpy, Btu/lb	0	10	16	20	24	28	34	40	46	52	57	66	79	105	149	151
		% water unfrozen	—	5	7	8	9	12	15	18	21	24	28	35	45	65	100	—
Peaches, without stones	85.1	Enthalpy, Btu/lb	0	10	16	20	24	28	34	42	47	53	59	67	81	108	148	150
		% water unfrozen	—	5	7	8	10	12	15	18	22	26	30	37	48	69	100	—
Pears, Barlett	83.8	Enthalpy, Btu/lb	0	10	17	21	25	29	35	42	47	53	59	69	83	111	146	148
		% water unfrozen	—	6	8	9	10	12	15	19	23	27	31	38	49	72	100	—
Plums, without stones	80.3	Enthalpy, Btu/lb	0	12	19	24	28	33	40	50	57	64	73	85	113	139	141	143
		% water unfrozen	—	8	11	13	16	18	22	28	34	38	46	55	71	100	—	—
Raspberries	82.7	Enthalpy, Btu/lb	0	10	16	19	22	26	31	38	42	46	52	59	71	92	146	148
		% water unfrozen	—	4	6	7	8	9	12	15	18	21	24	30	39	56	100	—
Spinach	90.2	Enthalpy, Btu/lb	0	8	14	16	19	22	26	29	32	35	38	42	48	59	93	158
		% water unfrozen	—	—	—	—	—	—	5	7	9	10	11	14	18	25	50	100
Strawberries	89.3	Enthalpy, Btu/lb	0	9	15	18	21	25	29	34	39	41	45	51	60	77	127	158
		% water unfrozen	—	—	—	5	6	7	8	10	13	15	18	21	28	40	79	100
Sweet cherries, without stones	77.0	Enthalpy, Btu/lb	0	12	20	24	29	35	42	51	59	67	76	89	110	134	136	138
		% water unfrozen	—	9	12	14	17	20	25	32	38	43	50	62	80	100	—	—
Tall peas	75.8	Enthalpy, Btu/lb	0	10	17	21	25	30	36	43	49	54	61	70	86	114	137	139
		% water unfrozen	—	6	8	10	12	15	18	22	27	30	37	44	57	82	100	—
Tomato pulp	92.9	Enthalpy, Btu/lb	0	10	14	17	20	23	27	32	36	39	42	47	54	68	112	163
		% water unfrozen	—	—	—	—	—	5	6	8	10	12	14	18	22	31	62	100
<b>Eggs</b>																		
Egg white	86.5	Enthalpy, Btu/lb	0	9	14	16	19	22	25	29	31	33	36	40	45	55	87	151
		% water unfrozen	—	—	—	—	—	—	—	—	10	12	13	14	17	22	48	100
Egg yolk	50.0	Enthalpy, Btu/lb	0	9	14	16	19	22	25	29	31	33	35	38	42	47	65	98
		% water unfrozen	—	—	—	—	—	—	—	—	—	—	20	23	27	32	66	100
Egg yolk	40.0	Enthalpy, Btu/lb	0	9	14	17	20	23	26	31	33	35	38	41	46	53	76	82
		% water unfrozen	20	—	—	—	24	—	27	—	30	—	34	38	43	54	89	100
Whole egg, w/shell <sup>a</sup>	66.4	Enthalpy, Btu/lb	0	9	13	15	18	20	23	27	29	31	34	37	41	49	73	121
<b>Fish and Meat</b>																		
Cod	80.3	Enthalpy, Btu/lb	0	10	15	18	21	24	28	33	36	39	43	48	56	73	123	139
		% water unfrozen	10	10	10	11	12	13	14	16	18	20	22	26	32	45	88	100
Haddock	83.6	Enthalpy, Btu/lb	0	9	15	18	21	24	28	33	36	39	43	48	56	73	127	145
		% water unfrozen	8	8	9	9	10	11	12	14	15	17	19	23	29	42	86	100
Perch	79.1	Enthalpy, Btu/lb	0	9	14	17	20	23	27	32	35	38	42	46	53	68	117	137
		% water unfrozen	10	10	11	11	12	13	14	16	17	19	21	24	30	41	83	100
Beef, lean, fresh <sup>b</sup>	74.5	Enthalpy, Btu/lb	0	9	15	18	21	24	27	32	35	38	42	48	57	74	119	131
		% water unfrozen	10	10	11	12	12	13	15	18	20	22	24	28	37	48	92	100
Beef, lean, dried	26.1	Enthalpy, Btu/lb	0	9	14	17	20	24	28	31	—	33	—	36	—	38	—	40
		% water unfrozen	96	96	96	97	98	99	100	—	—	—	—	—	—	—	—	—
<b>Bread</b>																		
White	37.3	Enthalpy, Btu/lb	0	9	13	15	18	21	26	34	40	45	51	55	56	57	58	59
Whole wheat	42.4	Enthalpy, Btu/lb	0	9	13	15	18	22	27	36	43	48	55	62	67	68	69	70

Source: Adapted from Dickerson (1968) and Riedel (1951, 1956, 1957, 1959).

<sup>b</sup>Calculated for a mass composition of 58% white (86.5% water) and 32% yolk (50% water).

<sup>c</sup>Data for chicken, veal, and venison nearly matched the data for beef of the same water content (Riedel 1957).

where  $k_c$  is the thermal conductivity of the continuous phase and  $L^3$  is the volume fraction of the discontinuous phase. In Equation (27), the thermal conductivity of the continuous phase is assumed to be much larger than the thermal conductivity of the discontinuous phase. However, if the thermal conductivity of the discontinuous phase is much larger than the thermal conductivity of the continuous phase, the following expression is used to calculate the thermal conductivity of the isotropic mixture:

$$k = k_c \left[ \frac{1 - M}{1 - M(1 - L)} \right] \quad (28)$$

where  $M = L^2(1 - k_d/k_c)$  and  $k_d$  is the thermal conductivity of the discontinuous phase.

For an anisotropic, two-component system in which the thermal conductivity depends on the direction of heat flow, such as in fibrous food materials, Kopelman (1966) developed two expressions for thermal conductivity. For heat flow parallel to the food fibers, Kopelman proposed the following expression for thermal conductivity  $k_{\parallel}$ :

$$k_{\parallel} = k_c \left[ 1 - N^2 \left( 1 - \frac{k_d}{k_c} \right) \right] \quad (29)$$

where  $N^2$  is the volume fraction of the discontinuous phase in the fibrous food product. If the heat flow is perpendicular to the food fibers, then the following expression for thermal conductivity  $k_{\perp}$  applies:

$$k_{\perp} = k_c \left[ \frac{1 - P}{1 - P(1 - N)} \right] \quad (30)$$

where  $P = N(1 - k_d/k_c)$ .

Levy (1981) introduced a modified version of the Maxwell-Eucken equation. Levy's expression for the thermal conductivity of a two-component system is as follows:

$$k = \frac{k_2[(2 + \Lambda) + 2(\Lambda - 1)F_1]}{(2 + \Lambda) - (\Lambda - 1)F_1} \quad (31)$$

where  $\Lambda$  is the thermal conductivity ratio ( $\Lambda = k_1/k_2$ ),  $k_1$  is the thermal conductivity of component 1, and  $k_2$  is the thermal conductivity of component 2. The parameter  $F_1$ , introduced by Levy is given as follows:

$$F_1 = 0.5 \left\{ \left( \frac{2}{\sigma} - 1 + 2R_1 \right) - \left[ \left( \frac{2}{\sigma} - 1 + 2R_1 \right)^2 - \frac{8R_1}{\sigma} \right]^{0.5} \right\} \quad (32)$$

where

$$\sigma = \frac{(\Lambda - 1)^2}{(\Lambda + 1)^2 + (\Lambda/2)} \quad (33)$$

and  $R_1$  is the volume fraction of component 1, or:

$$R_1 = \left[ 1 + \left( \frac{1}{x_1} - 1 \right) \left( \frac{\rho_1}{\rho_2} \right) \right]^{-1} \quad (34)$$

Here,  $x_1$  is the mass fraction of component 1,  $\rho_1$  is the density of component 1, and  $\rho_2$  is the density of component 2.

To use Levy's method, follow these steps:

1. Calculate the thermal conductivity ratio  $\Lambda$

2. Determine the volume fraction of constituent 1 using Equation (34)
3. Evaluate  $\sigma$  using Equation (33)
4. Determine  $F_1$  using Equation (32)
5. Evaluate the thermal conductivity of the two-component system via Equation (31)

When foods consist of more than two distinct phases, the previously mentioned methods for the prediction of thermal conductivity must be applied successively to obtain the thermal conductivity of the food product. For example, in the case of frozen food, the thermal conductivity of the ice and liquid water mix is calculated first by using one of the earlier methods mentioned. The resulting thermal conductivity of the ice/water mix is then combined successively with the thermal conductivity of each remaining food constituent to determine the thermal conductivity of the food product.

Numerous researchers have proposed the use of parallel and perpendicular (or series) thermal conductivity models based on analogies with electrical resistance (Murakami and Okos 1989). The parallel model is the sum of the thermal conductivities of the food constituents multiplied by their volume fractions:

$$k = \sum x_i^v k_i \quad (35)$$

where  $x_i^v$  is the volume fraction of constituent  $i$ . The volume fraction of constituent  $i$  can be found from the following equation:

$$x_i^v = \frac{x_i/\rho_i}{\sum (x_i/\rho_i)} \quad (36)$$

The perpendicular model is the reciprocal of the sum of the volume fractions divided by their thermal conductivities:

$$k = \frac{1}{\sum (x_i^v/k_i)} \quad (37)$$

These two models have been found to predict the upper and lower bounds of the thermal conductivity of most food items.

Tables 5 and 6 list the thermal conductivities for many food items (Qashou et al. 1972). Data in these tables have been averaged, interpolated, extrapolated, selected, or rounded off from the original research data. Tables 5 and 6 also include ASHRAE research data on foods of low and intermediate moisture content (Sweat 1985).

**Example 4.** Determine the thermal conductivity and density of lean pork shoulder meat which is at a temperature of  $-40^\circ\text{F}$ . Use both the parallel and perpendicular thermal conductivity models.

**Solution:**

From Table 3, the composition of lean pork shoulder meat is:

$$\begin{aligned} x_{wo} &= 0.7263 & x_f &= 0.0714 \\ x_p &= 0.1955 & x_a &= 0.0102 \end{aligned}$$

In addition, the initial freezing point of lean pork shoulder meat is  $28^\circ\text{F}$ . Because the temperature of the pork is below the initial freezing point, the fraction of ice within the pork must be determined. Using Equation (4), the ice fraction becomes:

$$\begin{aligned} x_{ice} &= (x_{wo} - x_b) \left[ 1 - \frac{t_f - 32}{t - 32} \right] = (x_{wo} - 0.4x_p) \left[ 1 - \frac{t_f - 32}{t - 32} \right] \\ &= [0.7263 - (0.4)(0.1955)] \left[ 1 - \frac{28 - 32}{-40 - 32} \right] = 0.6121 \end{aligned}$$

The mass fraction of unfrozen water is then:

$$x_w = x_{wo} - x_{ice} = 0.7263 - 0.6121 = 0.1142$$

Table 5 Thermal Conductivity of Foods

Food Item <sup>a</sup>	Thermal Conductivity Btu/h·ft·°F	Temperature, °F	Water Content, % by mass	Reference <sup>b</sup>	Remarks
<b>Fruits, Vegetables</b>					
Apples	0.242	46.4	—	Gane (1936)	Tasmanian French crabapple, whole fruit; 0.3 lb
Apples, dried	0.127	73.4	41.6	Sweat (1985)	Density = 54 lb/ft <sup>3</sup>
Apple juice	0.323	68	87	Riedel (1949)	Refractive index at 68°F = 1.35
	0.365	176	87		
	0.291	68	70		Refractive index at 68°F = 1.38
	0.326	176	70		
	0.225	68	36		Refractive index at 68°F = 1.45
	0.251	176	36		
Apple sauce	0.317	84.2	—	Sweat (1974)	
Apricots, dried	0.217	73.4	43.6	Sweat (1985)	Density = 82 lb/ft <sup>3</sup>
Beans, runner	0.230	48.2	—	Smith et al. (1952)	Density = 47 lb/ft <sup>3</sup> ; machine sliced, scalded, packed in slab
Beets	0.347	82.4	87.6	Sweat (1974)	
Broccoli	0.222	21.2	—	Smith et al. (1952)	Density = 35 lb/ft <sup>3</sup> ; heads cut and scalded
Carrots	0.387	3.2	—	Smith et al. (1952)	Density = 37 lb/ft <sup>3</sup> ; scraped, sliced and scalded
Carrots, puree	0.728	17.6	—	Smith et al. (1952)	Density = 56 lb/ft <sup>3</sup> ; slab
Currants, black	0.179	1.4	—	Smith et al. (1952)	Density = 40 lb/ft <sup>3</sup>
Dates	0.195	73.4	34.5	Sweat (1985)	Density = 82 lb/ft <sup>3</sup>
Figs	0.179	73.4	40.4	Sweat (1985)	Density = 77 lb/ft <sup>3</sup>
Gooseberries	0.159	5	—	Smith et al. (1952)	Density = 36 lb/ft <sup>3</sup> ; mixed sizes
Grapefruit juice vesicle	0.267	86	—	Bennett et al. (1964)	Marsh, seedless
Grapefruit rind	0.137	82	—	Bennett et al. (1964)	Marsh, seedless
Grape, green, juice	0.328	68	89	Riedel (1949)	Refractive index at 68°F = 1.35
	0.369	176	89		
	0.287	68	68		Refractive index at 68°F = 1.38
	0.320	176	68		
	0.229	68	37		Refractive index at 20°C = 1.45
	0.254	176	37		
	0.254	77	—	Turrell and Perry (1957)	Eureka
Grape jelly	0.226	68	42.0	Sweat (1985)	Density = 82 lb/ft <sup>3</sup>
Nectarines	0.338	47.5	82.9	Sweat (1974)	
Onions	0.332	47.5	—	Saravacos (1965)	
Orange juice vesicle	0.251	86	—	Bennett et al. (1964)	Valencia
Orange rind	0.103	86	—	Bennett et al. (1964)	Valencia
Peas	0.277	8.6	—	Smith et al. (1952)	Density = 44 lb/ft <sup>3</sup> ; shelled and scalded
	0.228	26.6	—		
	0.182	44.6	—		
Peaches, dried	0.209	73.4	43.4	Sweat (1985)	Density = 79 lb/ft <sup>3</sup>
Pears	0.344	47.7	—	Sweat (1974)	
Pear juice	0.318	68	85	Riedel (1949)	Refractive index at 68°F = 1.36
	0.363	176	85		
	0.274	68	60		Refractive index at 68°F = 1.40
	0.307	176	60		
	0.232	68	39		Refractive index at 68°F = 1.44
	0.258	176	39		
Plums	0.143	3.2	—	Smith et al. (1952)	Density = 38 lb/ft <sup>3</sup> ; 1.57 in. dia.; 2.0 in. long
Potatoes, mashed	0.630	8.6	—	Smith et al. (1952)	Density = 61 lb/ft <sup>3</sup> ; tightly packed slab
Potato salad	0.277	35.6	—	Dickerson and Read (1968)	Density = 63 lb/ft <sup>3</sup>
Prunes	0.217	73.4	42.9	Sweat (1985)	Density = 76 lb/ft <sup>3</sup>
Raisins	0.194	73.4	32.2	Sweat (1985)	Density = 86 lb/ft <sup>3</sup>
Strawberries	0.636	6.8	—	Smith et al. (1952)	Mixed sizes, density = 50 lb/ft <sup>3</sup> , slab
	0.555	5	—		Mixed sizes in 57% sucrose syrup, slab
Strawberry, jam	0.195	68	41.0	Sweat (1985)	Density = 82 lb/ft <sup>3</sup>
Squash	0.290	46.4	—	Gane (1936)	
<b>Meat and Animal Byproducts</b>					
Beef brain	0.287	95	77.7	Poppendick et al. (1966)	12% fat; 10.3% protein; density = 63 lb/ft <sup>3</sup>
Beef fat	0.110	95	0.0	Poppendick et al. (1966)	Melted 100% fat; density = 51 lb/ft <sup>3</sup>
	0.133	95	20		Density = 54 lb/ft <sup>3</sup>
Beef fat ⊥ <sup>a</sup>	0.125	35.6	9	Lentz (1961)	89% fat
	0.166	15.8	9		
Beef kidney	0.303	95	76.4	Poppendick et al. (1966)	8.3% fat, 15.3% protein; density = 64 lb/ft <sup>3</sup>
Beef liver	0.282	95	72	Poppendick et al. (1966)	7.2% fat, 20.6% protein
Beef, lean = <sup>a</sup>	0.292	37.4	75	Lentz (1961)	Sirloin; 0.9% fat
	0.820	5	75		
Beef, lean = <sup>a</sup>	0.248	68	79	Hill et al. (1967)	1.4% fat
	0.826	5	79		
Beef, lean = <sup>a</sup>	0.231	42.8	76.5	Hill et al. (1967), Hill (1966)	2.4% fat
	0.786	5	76.5		
Beef, lean ⊥ <sup>a</sup>	0.277	68	79	Hill et al. (1967)	Inside round; 0.8% fat
	0.780	5	79		
Beef, lean ⊥ <sup>a</sup>	0.237	42.8	76	Hill et al. (1967), Hill (1966)	3% fat
	0.659	5	76		
Beef, lean ⊥ <sup>a</sup>	0.272	37.4	74	Lentz (1961)	Flank; 3 to 4% fat
	0.647	5	74		
Beef, ground	0.235	42.8	67	Qashou et al. (1970)	12.3% fat; density = 59 lb/ft <sup>3</sup>
	0.237	39.2	62		16.8% fat; density = 61 lb/ft <sup>3</sup>
	0.203	42.8	55		18% fat; density = 58 lb/ft <sup>3</sup>

Table 5 Thermal Conductivity of Foods (Continued)

Food Item <sup>a</sup>	Thermal Conductivity Btu/h·ft·°F	Temperature, °F	Water Content, % by mass	Reference <sup>b</sup>	Remarks
	0.210	37.4	53		22% fat; density = 59 lb/ft <sup>3</sup>
Beefstick	0.172	68	36.6	Sweat (1985)	Density = 66 lb/ft <sup>3</sup>
Bologna	0.243	68	64.7	Sweat (1985)	Density = 62 lb/ft <sup>3</sup>
Dog food	0.184	73.4	30.6	Sweat (1985)	Density = 77 lb/ft <sup>3</sup>
Cat food	0.188	73.4	39.7	Sweat (1985)	Density = 71 lb/ft <sup>3</sup>
Ham, country	0.277	68	71.8	Sweat (1985)	Density = 64 lb/ft <sup>3</sup>
Horse meat <sub>L</sub> <sup>a</sup>	0.266	86	70	Griffiths and Cole (1948)	Lean
Lamb <sub>L</sub> <sup>a</sup>	0.263	68	72	Hill et al. (1967)	8.7% fat
	0.647	5	72		
Lamb = <sup>a</sup>	0.231	68	71	Hill et al. (1967)	9.6% fat
	0.734	5	71		
Pepperoni	0.148	68	32.0	Sweat (1985)	Density = 66 lb/ft <sup>3</sup>
Pork fat	0.124	37.4	6	Lentz (1961)	93% fat
	0.126	5	6		
Pork, lean flank	0.266	36.0	—	Lentz (1961)	3.4% fat
	0.705	5	—		
Pork, lean leg = <sup>a</sup>	0.276	39.2	72	Lentz (1961)	6.1% fat
	0.861	5	72		
Pork, lean = <sup>a</sup>	0.262	68	76	Hill et al. (1967)	6.7% fat
	0.820	8.6	76		
Pork, lean leg ⊥ <sup>a</sup>	0.263	39.2	72	Lentz (1961)	6.1% fat
	0.745	5	72		
Pork, lean ⊥ <sup>a</sup>	0.292	68	76	Hill et al. (1967)	6.7% fat
	0.751	6.8	76		
Salami	0.180	68	35.6	Sweat (1985)	Density = 60 lb/ft <sup>3</sup>
Sausage	0.247	77	68	Woodams (1965), Nowrey and Woodams (1968)	Mixture of beef and pork; 16.1% fat, 12.2% protein
	0.222	77	62		Mixture of beef and pork; 24.1% fat, 10.3% protein
Veal ⊥ <sup>a</sup>	0.272	68	75	Hill et al. (1967)	2.1% fat
	0.797	5	75		
Veal = <sup>a</sup>	0.257	82.4	75	Hill et al. (1967)	2.1% fat
	0.844	5	75		
<b>Poultry and Eggs</b>					
Chicken breast <sub>L</sub> <sup>a</sup>	0.238	68	69–75	Walters and May (1963)	0.6% fat
Chicken breast with skin	0.211	68	58–74	Walters and May (1963)	0–30% fat
Turkey breast ⊥ <sup>a</sup>	0.287	37.4	74	Lentz (1961)	2.1% fat
	0.797	5	74		
Turkey leg ⊥ <sup>a</sup>	0.287	39.2	74	Lentz (1961)	3.4% fat
	0.711	5	74		
Turkey breast = ⊥ <sup>a</sup>	0.290	37.4	74	Lentz (1961)	2.1% fat
	0.884	5	74		
Egg white	0.322	96.8	88	Spells (1960–61), Spells (1958)	
Egg, whole	0.555	17.6	—	Smith et al. (1952)	Density = 61 lb/ft <sup>3</sup>
Egg yolk	0.243	87.8	50.6	Poppendick et al. (1966)	32.7% fat; 16.7% protein, density = 64 lb/ft <sup>3</sup>
<b>Fish and Sea Products</b>					
Fish, cod ⊥ <sup>a</sup>	0.309	37.4	83	Lentz (1961)	0.1% fat
	0.844	5	83		
Fish, cod	0.324	33.8	—	Long (1955), Jason and Long (1955)	
	0.976	5	—	Long (1955)	
Fish, herring	0.462	-2.2	—	Smith et al. (1952)	Density = 57 lb/ft <sup>3</sup> ; whole and gutted
Fish, salmon ⊥ <sup>a</sup>	0.307	37.4	67	Lentz (1961)	12% fat; <i>Salmo salar</i> from Gaspé peninsula
	0.716	5	67		
Fish, salmon ⊥ <sup>a</sup>	0.288	41	73	Lentz (1961)	5.4% fat; <i>Oncorhynchus tshawytscha</i> from British Columbia
	0.653	5	73		
Seal blubber ⊥ <sup>a</sup>	0.114	41	4.3	Lentz (1961)	95% fat
Whale blubber ⊥ <sup>a</sup>	0.121	64.4	—	Griffiths and Cole (1948)	Density = 65 lb/ft <sup>3</sup>
Whale meat	0.375	89.6	—	Griffiths and Hickman (1951)	Density = 67 lb/ft <sup>3</sup>
	0.832	15.8	—		
	0.740	10.4	—	Smith et al. (1952)	0.51% fat; density = 62 lb/ft <sup>3</sup>
<b>Dairy Products</b>					
Butterfat	0.100	42.8	0.6	Lentz (1961)	
	0.103	5	0.6		
Butter	0.114	39.2	—	Hooper and Chang (1952)	
Buttermilk	0.329	68	89	Riedel (1949)	0.35% fat
Milk, whole	0.335	82.4	90	Leidenfrost (1959)	3% fat
	0.302	35.6	83	Riedel (1949)	3.6% fat
	0.318	68	83		
	0.339	122	83		
	0.355	176	83		
Milk, skimmed	0.311	35.6	90	Riedel (1949)	0.1% fat
	0.327	68	90		
	0.350	122	90		
	0.367	176	90		
Milk, evaporated	0.281	35.6	72	Riedel (1949)	4.8% fat
	0.291	68	72		
	0.313	122	72		
	0.326	176	72		
Milk, evaporated	0.263	35.6	62	Riedel (1949)	6.4% fat

Table 5 Thermal Conductivity of Foods (Continued)

Food Item <sup>a</sup>	Thermal Conductivity Btu/h·ft·°F	Temperature, °F	Water Content, % by mass	Reference <sup>b</sup>	Remarks
Whey	0.273	68	62	Leidenfrost (1959)	10% fat
	0.295	122	62		
	0.307	176	62		
	0.273	73.4	67		
	0.291	105.8	67		
	0.298	140	67		
	0.304	174.2	67	Leidenfrost (1959)	15% fat
	0.187	78.8	50		
	0.196	104	50		
	0.206	138.2	50	Riedel (1949)	No fat
	0.210	174.2	50		
	0.312	35.6	90		
	0.328	68	90		
0.364	122	90			
0.370	176	90			
<b>Sugar, Starch, Bakery Products, and Derivatives</b>					
Sugar beet juice	0.318	77	79	Khelemskii and Zhadan (1964)	
Sucrose solution	0.329	77	82	Riedel (1949)	Cane or beet sugar solution
	0.309	32	90		
	0.327	68	90		
	0.351	122	90		
	0.367	176	90		
	0.291	32	80		
	0.309	68	80		
	0.330	122	80		
	0.347	176	80		
	0.273	32	70		
	0.289	68	70		
	0.310	122	70		
	0.325	176	70		
	0.256	32	60		
	0.272	68	60		
	0.290	122	60		
	0.303	176	60		
	0.239	32	50		
	0.252	68	50		
	0.270	122	93–80		
0.283	176	93–80			
0.221	32	40	Riedel (1949)		
0.233	68	40			
0.251	122	40			
0.262	176	40			
0.311	35.6	89			
0.327	68	89			
0.347	122	89			
0.369	176	89			
0.294	35.6	80			
0.309	68	80			
0.330	122	80			
0.346	176	80			
0.276	35.6	70			
0.291	68	70			
0.311	122	70			
0.326	176	70			
0.258	35.6	60			
0.272	68	60			
0.289	122	60			
0.306	176	60			
Corn syrup	0.325	77	—	Metzner and Friend (1959)	Density = 72 lb/ft <sup>3</sup> Density = 82 lb/ft <sup>3</sup> Density = 84 lb/ft <sup>3</sup>
	0.280	77	—		
	0.270	77	—		
Honey	0.290	35.6	80	Reidy (1968)	
	0.240	156.2	80		
Molasses syrup	0.200	86	23	Popov and Terentiev (1966)	
Angel food cake	0.057	73.4	36.1	Sweat (1985)	Density = 9.4 lb/ft <sup>3</sup> , porosity: 88%
Applesauce cake	0.046	73.4	23.7	Sweat (1985)	Density = 19 lb/ft <sup>3</sup> , porosity: 78%
Carrot cake	0.049	73.4	21.6	Sweat (1985)	Density = 20 lb/ft <sup>3</sup> , porosity: 75%
Chocolate cake	0.061	73.4	31.9	Sweat (1985)	Density = 21 lb/ft <sup>3</sup> , porosity: 74%
Pound cake	0.076	73.4	22.7	Sweat (1985)	Density = 30 lb/ft <sup>3</sup> , porosity: 58%
Yellow cake	0.064	73.4	25.1	Sweat (1985)	Density = 19 lb/ft <sup>3</sup> , porosity: 78%
White cake	0.047	73.4	32.3	Sweat (1985)	Density = 28 lb/ft <sup>3</sup> , porosity: 62%
<b>Grains, Cereals, and Seeds</b>					
Corn, yellow	0.081	89.6	0.9	Kazarian (1962)	Density = 47 lb/ft <sup>3</sup> Density = 47 lb/ft <sup>3</sup> Density = 42 lb/ft <sup>3</sup>
	0.092	89.6	14.7		
	0.099	89.6	30.2		
Flax seed	0.066	89.6	—	Griffiths and Hickman (1951)	Density = 41 lb/ft <sup>3</sup>
Oats, white English	0.075	80.6	12.7	Oxley (1944)	
Sorghum	0.076	41	13	Miller (1963)	Hybrid Rs610 grain

Table 5 Thermal Conductivity of Foods (Continued)

Food Item <sup>a</sup>	Thermal Conductivity Btu/h·ft·°F	Temperature, °F	Water Content, % by mass	Reference <sup>b</sup>	Remarks
	0.087		22		
Wheat, No. 1, Northern hard spring	0.078	93.2	2	Moote (1953)	Values taken from plot of series of values given by authors
	0.086	—	7	Babbitt (1945)	
	0.090	—	10		
	0.097	—	14		
Wheat, soft white winter	0.000	32			Values taken from plot of series of values given by author; Density = 49 lb/ft <sup>3</sup>
	0.070	87.8	5	Kazarian (1962)	
	0.075	87.8	10		
	0.079	87.8	15		
<b>Fats, Oils, Gums, and Extracts</b>					
Gelatin gel	0.302	41	94–80	Lentz (1961)	Conductivity did not vary with concentration in range tested (6, 12, 20%)
	1.236	5	94		6% gelatin concentration
	1.121	5	88		12% gelatin concentration
	0.815	5	80		20% gelatin concentration
Margarine	0.135	41	—	Hooper and Chang (1952)	Density = 62 lb/ft <sup>3</sup>
Almond oil	0.102	39.2	—	Wachsmuth (1892)	Density = 57 lb/ft <sup>3</sup>
Cod liver oil	0.098	95	—	Spells (1960-61), Spells (1958)	
Lemon oil	0.090	42.8	—	Weber (1880)	Density = 51 lb/ft <sup>3</sup>
Mustard oil	0.098	77	—	Weber (1886)	Density = 64 lb/ft <sup>3</sup>
Nutmeg oil	0.090	39.2	—	Wachsmuth (1892)	Density = 59 lb/ft <sup>3</sup>
Olive oil	0.101	44.6	—	Weber (1880)	Density = 57 lb/ft <sup>3</sup>
Olive oil	0.097	89.6	—	Kaye and Higgins (1928)	Density = 57 lb/ft <sup>3</sup>
	0.096	149	—		
	0.092	304	—		
	0.090	365	—		
Peanut oil	0.097	39.2	—	Wachsmuth (1892)	Density = 57 lb/ft <sup>3</sup>
Peanut oil	0.098	77	—	Woodams (1965)	
Rapeseed oil	0.092	68	—	Kondrat'ev (1950)	Density = 57 lb/ft <sup>3</sup>
Sesame oil	0.102	39.2	—	Wachsmuth (1892)	Density = 57 lb/ft <sup>3</sup>

<sup>a</sup>The symbol ⊥ indicates heat flow perpendicular to the grain structure and the symbol = indicates heat flow parallel to the grain or structure.

<sup>b</sup>References quoted are those on which given data are based, although actual values in this table may have been averaged, interpolated, extrapolated, selected, or rounded off.

Table 6 Thermal Conductivity of Freeze-Dried Foods

Food Item	Thermal Conductivity, Btu/h·ft·°F	Temperature, °F	Pressure, psia	Reference <sup>b</sup>	Remarks
Apple	0.0090	95	0.000386	Harper (1960, 1962)	Delicious; 88% porosity; 5.1 tortuosity factor; measured in air
	0.0107	95	0.00305		
	0.0163	95	0.0271		
	0.0234	95	0.418		
Peach	0.0095	95	0.000870	Harper (1960, 1962)	Clingstone; 91% porosity; 4.1 tortuosity factor; measured in air
	0.0107	95	0.00312		
	0.0161	95	0.0271		
	0.0237	95	0.387		
	0.0249	95	7.40		
Pears	0.0107	95	0.000309	Harper (1960, 1962)	97% porosity; measured in nitrogen
	0.0120	95	0.00283		
	0.0177	95	0.0271		
	0.0242	95	0.312		
	0.0261	95	10.0		
Beef = <sup>a</sup>	0.0221	95	0.000212	Harper (1960, 1962)	Lean; 64% porosity; 4.4 tortuosity factor; measured in air
	0.0238	95	0.00329		
	0.0307	95	0.0345		
	0.0358	95	0.392		
	0.0377	95	14.7		
Egg albumin gel	0.0227	106	14.7	Saravacos and Pilsworth (1965)	2% water content; measured in air
	0.0075	106	0.00064	Saravacos and Pilsworth (1965)	
Turkey = <sup>a</sup>	0.0166	—	0.000773	Triebes and King (1966)	Cooked white meat; 68 to 72% porosity; measured in air
	0.0256	—	0.00218		
	0.0408	—	0.0677		
	0.0497	—	0.309		
	0.0536	—	14.3		
Turkey ⊥ <sup>a</sup>	0.0098	—	0.000812	Triebes and King (1966)	Cooked white meat; 68 to 72% porosity; measured in air
	0.0101	—	0.00274		
	0.0128	—	0.0193		
	0.0241	—	0.181		
	0.0339	—	12.7		
Potato starch gel	0.0053	—	0.000624	Saravacos and Pilsworth (1965)	Measured in air
	0.0083	—	0.0262		
	0.0168	—	0.320		
	0.0227	—	14.9		

<sup>a</sup>The symbol ⊥ indicates heat flow perpendicular to the grain structure and the symbol = indicates heat flow parallel to the grain or structure.

<sup>b</sup>References quoted are those on which given data are based, although actual values in this table may have been averaged, interpolated, extrapolated, selected, or rounded off.

Using the equations presented in Tables 1 and 2, the density and thermal conductivity of the food constituents are calculated at the given temperature  $-40^{\circ}\text{F}$ :

$$\begin{aligned}\rho_w &= 6.2174 \times 10^1 + 4.7425 \times 10^{-3}(-40) - 7.2397 \times 10^{-5}(-40)^2 \\ &= 61.868 \text{ lb/ft}^3\end{aligned}$$

$$\begin{aligned}\rho_{ice} &= 5.7385 \times 10^1 - 4.5333 \times 10^{-3}(-40) \\ &= 57.566 \text{ lb/ft}^3\end{aligned}$$

$$\begin{aligned}\rho_p &= 8.3599 \times 10^1 - 1.7979 \times 10^{-2}(-40) \\ &= 84.318 \text{ lb/ft}^3\end{aligned}$$

$$\begin{aligned}\rho_f &= 5.8246 \times 10^1 - 1.4482 \times 10^{-2}(-40) \\ &= 58.825 \text{ lb/ft}^3\end{aligned}$$

$$\begin{aligned}\rho_a &= 1.5162 \times 10^2 - 9.7329 \times 10^{-3}(-40) \\ &= 152.01 \text{ lb/ft}^3\end{aligned}$$

$$\begin{aligned}k_w &= 3.1064 \times 10^{-1} + 6.4226 \times 10^{-4}(-40) - 1.1955 \times 10^{-6}(-40)^2 \\ &= 0.2830 \text{ Btu/(h}\cdot\text{ft}\cdot^{\circ}\text{F)}\end{aligned}$$

$$\begin{aligned}k_{ice} &= 1.3652 - 3.1648 \times 10^{-3}(-40) + 1.8108 \times 10^{-5}(-40)^2 \\ &= 1.521 \text{ Btu/(h}\cdot\text{ft}\cdot^{\circ}\text{F)}\end{aligned}$$

$$\begin{aligned}k_p &= 9.0535 \times 10^{-2} + 4.1486 \times 10^{-4}(-40) - 4.8467 \times 10^{-7}(-40)^2 \\ &= 0.07317 \text{ Btu/(h}\cdot\text{ft}\cdot^{\circ}\text{F)}\end{aligned}$$

$$\begin{aligned}k_f &= 1.3273 \times 10^{-1} - 8.8405 \times 10^{-4}(-40) - 3.1652 \times 10^{-8}(-40)^2 \\ &= 0.1680 \text{ Btu/(h}\cdot\text{ft}\cdot^{\circ}\text{F)}\end{aligned}$$

$$\begin{aligned}k_a &= 1.7553 \times 10^{-1} + 4.8292 \times 10^{-4}(-40) - 5.1839 \times 10^{-7}(-40)^2 \\ &= 0.1554 \text{ Btu/(h}\cdot\text{ft}\cdot^{\circ}\text{F)}\end{aligned}$$

Using Equation (6), the density of the lean pork shoulder meat at  $-40^{\circ}\text{F}$  can be determined:

$$\begin{aligned}\sum \frac{x_i}{\rho_i} &= \frac{0.6121}{57.566} + \frac{0.1142}{61.868} + \frac{0.1955}{84.318} + \frac{0.0714}{58.825} + \frac{0.0102}{152.01} \\ &= 1.6078 \times 10^{-2} \\ \rho &= \frac{1 - \epsilon}{\sum x_i/\rho_i} = \frac{1 - 0}{1.6078 \times 10^{-2}} = 62.2 \text{ lb/ft}^3\end{aligned}$$

Using Equation (36), the volume fractions of the constituents can be found:

$$x_{ice}^v = \frac{x_{ice}/\rho_{ice}}{\sum x_i/\rho_i} = \frac{0.6121/57.566}{1.6078 \times 10^{-2}} = 0.6613$$

$$x_w^v = \frac{x_w/\rho_w}{\sum x_i/\rho_i} = \frac{0.1142/61.868}{1.6078 \times 10^{-2}} = 0.1148$$

$$x_p^v = \frac{x_p/\rho_p}{\sum x_i/\rho_i} = \frac{0.1955/84.318}{1.6078 \times 10^{-2}} = 0.1442$$

$$x_f^v = \frac{x_f/\rho_f}{\sum x_i/\rho_i} = \frac{0.0714/58.825}{1.6078 \times 10^{-2}} = 0.0755$$

$$x_a^v = \frac{x_a/\rho_a}{\sum x_i/\rho_i} = \frac{0.0102/152.01}{1.6078 \times 10^{-2}} = 0.0042$$

Using the parallel model, Equation (35), the thermal conductivity becomes:

$$\begin{aligned}k &= \sum x_i^v k_i = (0.6613)(1.521) + (0.1148)(0.2830) \\ &\quad + (0.1442)(0.0731) + (0.0755)(0.1680) + (0.0042)(0.1554) \\ k &= 1.06 \text{ Btu/(h}\cdot\text{ft}\cdot^{\circ}\text{F)}\end{aligned}$$

Using the perpendicular model, Equation (37), the thermal conductivity becomes:

$$\begin{aligned}k &= \frac{1}{\sum x_i^v/k_i} = \left[ \frac{0.6613}{1.521} + \frac{0.1148}{0.2830} + \frac{0.1442}{0.07317} + \frac{0.0755}{0.1680} + \frac{0.0042}{0.1554} \right]^{-1} \\ k &= 0.304 \text{ Btu/(h}\cdot\text{ft}\cdot^{\circ}\text{F)}\end{aligned}$$

**Example 5.** Determine the thermal conductivity and density of lean pork shoulder meat which is at a temperature of  $-40^{\circ}\text{F}$ . Use the isotropic model developed by Kopelman (1966).

**Solution:**

From Table 3, the composition of lean pork shoulder meat is:

$$\begin{aligned}x_{wo} &= 0.7263x_f = 0.0714 \\ x_p &= 0.1955x_a = 0.0102\end{aligned}$$

In addition, the initial freezing point of lean pork shoulder is  $28^{\circ}\text{F}$ . Because the temperature of the pork is below the initial freezing point, the fraction of ice within the pork must be determined. From Example 4, the ice fraction was found to be:

$$x_{ice} = 0.6121$$

The mass fraction of unfrozen water is then:

$$x_w = x_{wo} - x_{ice} = 0.7263 - 0.6121 = 0.1142$$

Using the equations presented in Tables 1 and 2, the density and thermal conductivity of the food constituents are calculated at the given temperature,  $-40^{\circ}\text{F}$  (refer to Example 4):

$$\begin{aligned}\rho_w &= 61.868 \text{ lb/ft}^3 & k_w &= 0.2830 \text{ Btu/(h}\cdot\text{ft}\cdot^{\circ}\text{F)} \\ \rho_{ice} &= 57.566 \text{ lb/ft}^3 & k_{ice} &= 1.521 \text{ Btu/(h}\cdot\text{ft}\cdot^{\circ}\text{F)} \\ \rho_p &= 84.318 \text{ lb/ft}^3 & k_p &= 0.07317 \text{ Btu/(h}\cdot\text{ft}\cdot^{\circ}\text{F)} \\ \rho_f &= 58.825 \text{ lb/ft}^3 & k_f &= 0.1680 \text{ Btu/(h}\cdot\text{ft}\cdot^{\circ}\text{F)} \\ \rho_a &= 152.01 \text{ lb/ft}^3 & k_a &= 0.1554 \text{ Btu/(h}\cdot\text{ft}\cdot^{\circ}\text{F)}\end{aligned}$$

Now, determine the thermal conductivity of the ice/water mixture. This requires the volume fractions of the ice and the water in the two component ice/water mixture:

$$\begin{aligned}x_w^v &= \frac{x_w/\rho_w}{\sum \frac{x_i}{\rho_i}} = \frac{0.1142/61.868}{\frac{0.1142}{61.868} + \frac{0.6121}{57.566}} = 0.1479 \\ x_{ice}^v &= \frac{x_{ice}/\rho_{ice}}{\sum \frac{x_i}{\rho_i}} = \frac{0.6121/57.566}{\frac{0.1142}{61.868} + \frac{0.6121}{57.566}} = 0.8521\end{aligned}$$

Note that the volume fractions calculated for the two component ice/water mixture are different from those calculated in Example 4 for the lean pork shoulder meat. Because the ice has the largest volume fraction in the two component ice/water mixture, consider the ice to be the "continuous" phase. Then,  $L$  from Equation (27) becomes:

$$\begin{aligned}L^3 &= x_w^v = 0.1479 \\ L^2 &= 0.2797 \\ L &= 0.5288\end{aligned}$$

Because  $k_{ice} > k_w$  and the ice is the continuous phase, the thermal conductivity of the ice/water mixture is calculated using Equation (27):

$$\begin{aligned}k_{ice/water} &= k_{ice} \left[ \frac{1 - L^2}{1 - L^2(1 - L)} \right] \\ &= 1.521 \left[ \frac{1 - 0.2797}{1 - 0.2797(1 - 0.5288)} \right] = 1.2619 \text{ Btu/(h}\cdot\text{ft}\cdot^{\circ}\text{F)}\end{aligned}$$

The density of the ice/water mixture then becomes:

$$\begin{aligned}\rho_{ice/water} &= x_w^v \rho_w + x_{ice}^v \rho_{ice} \\ &= (0.1479)(61.868) + (0.8521)(57.566) \\ &= 58.202 \text{ lb/ft}^3\end{aligned}$$



Next, find the thermal conductivity of the ice/water/protein mixture. This requires the volume fractions of the ice/water and the protein:

$$x_p^v = \frac{x_p/\rho_p}{\sum \frac{x_i}{\rho_i}} = \frac{0.1955/84.318}{\frac{0.1955}{84.318} + \frac{0.7263}{58.202}} = 0.1567$$

$$x_{ice/water}^v = \frac{x_{ice/water}/\rho_{ice/water}}{\sum \frac{x_i}{\rho_i}} = \frac{0.7263/58.202}{\frac{0.1955}{84.318} + \frac{0.7263}{58.202}} = 0.8433$$

Note that these volume fractions are calculated based on a two component system composed of ice/water as one constituent and protein as the other. Because protein has the smaller volume fraction, consider it to be the discontinuous phase.

$$L^3 = x_p^v = 0.1567$$

$$L^2 = 0.2907$$

$$L = 0.5391$$

Thus, the thermal conductivity of the ice/water/protein mixture becomes:

$$\begin{aligned} k_{ice/water/protein} &= k_{ice/water} \left[ \frac{1-L^2}{1-L^2(1-L)} \right] \\ &= 1.2619 \left[ \frac{1-0.2907}{1-0.2907(1-0.5391)} \right] \\ &= 0.942 \text{ Btu/h}\cdot\text{ft}\cdot^\circ\text{F} \end{aligned}$$

The density of the ice/water/protein mixture then becomes:

$$\begin{aligned} \rho_{ice/water/protein} &= x_{ice/water}^v \rho_{ice/water} + x_p^v \rho_p \\ &= (0.8433)(58.202) + (0.1567)(84.318) \\ &= 62.294 \text{ lb/ft}^3 \end{aligned}$$

Next, find the thermal conductivity of the ice/water/protein/fat mixture. This requires the volume fractions of the ice/water/protein and the fat:

$$x_f^v = \frac{x_f/\rho_f}{\sum \frac{x_i}{\rho_i}} = \frac{0.0714/58.825}{\frac{0.0714}{58.825} + \frac{0.9218}{62.294}} = 0.0758$$

$$x_{i/w/p}^v = \frac{x_{i/w/p}/\rho_{i/w/p}}{\sum \frac{x_i}{\rho_i}} = \frac{0.9218/62.294}{\frac{0.0714}{58.825} + \frac{0.9218}{62.294}} = 0.9242$$

$$L^3 = x_f^v = 0.0758$$

$$L^2 = 0.1791$$

$$L = 0.4232$$

Thus, the thermal conductivity of the ice/water/protein/fat mixture becomes:

$$\begin{aligned} k_{i/w/p/f} &= k_{i/w/p} \left[ \frac{1-L^2}{1-L^2(1-L)} \right] \\ &= 1.0335 \left[ \frac{1-0.1791}{1-0.1791(1-0.4232)} \right] \\ &= 0.9461 \text{ Btu/(h}\cdot\text{ft}\cdot^\circ\text{F)} \end{aligned}$$

The density of the ice/water/protein/fat mixture then becomes:

$$\begin{aligned} \rho_{i/w/p/f} &= x_{i/w/p}^v \rho_{i/w/p} + x_f^v \rho_f \\ &= (0.9242)(62.294) + (0.0758)(58.825) \\ &= 62.031 \text{ lb/ft}^3 \end{aligned}$$

Finally, the thermal conductivity of the lean pork shoulder meat can be found. This requires the volume fractions of the ice/water/protein/fat and the ash:

$$x_a^v = \frac{x_a/\rho_a}{\sum \frac{x_i}{\rho_i}} = \frac{0.0102/152.01}{\frac{0.0102}{152.01} + \frac{0.9932}{62.031}} = 0.0042$$

$$x_{i/w/p/f}^v = \frac{x_{i/w/p/f}}{\sum \frac{x_i}{\rho_i}} = \frac{\frac{0.9932}{62.031}}{\frac{0.0102}{152.01} + \frac{0.9932}{62.031}} = 0.9958$$

$$L^3 = x_a^v = 0.0042$$

$$L^2 = 0.0260$$

$$L = 0.1613$$

Thus, the thermal conductivity of the lean pork shoulder meat becomes:

$$\begin{aligned} k_{pork} &= k_{i/w/p/f} \left[ \frac{1-L^2}{1-L^2(1-L)} \right] \\ &= 0.9461 \left[ \frac{1-0.0260}{1-0.0260(1-0.1613)} \right] \\ &= 0.942 \text{ Btu/(h}\cdot\text{ft}\cdot^\circ\text{F)} \end{aligned}$$

The density of the lean pork shoulder meat then becomes:

$$\begin{aligned} \rho_{pork} &= x_{i/w/p/f}^v \rho_{i/w/p/f} + x_a^v \rho_a \\ &= (0.9958)(62.031) + (0.0042)(152.01) \\ &= 62.4 \text{ lb/ft}^3 \end{aligned}$$

### THERMAL DIFFUSIVITY

For transient heat transfer, the important thermophysical property is thermal diffusivity  $\alpha$ , which appears in the Fourier equation:

$$\frac{\partial T}{\partial \theta} = \alpha \left[ \frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} + \frac{\partial^2 T}{\partial z^2} \right] \quad (38)$$

where  $x, y, z$  are rectangular coordinates,  $T$  is temperature, and  $\theta$  is time. Thermal diffusivity can be defined as follows:

$$\alpha = \frac{k}{\rho c} \quad (39)$$

where  $\alpha$  is thermal diffusivity,  $k$  is thermal conductivity,  $\rho$  is density, and  $c$  is specific heat.

Experimentally determined values of the thermal diffusivity of foods are scarce. However, thermal diffusivity can be calculated using Equation (39), with appropriate values of thermal conductivity, specific heat, and density. A few experimental values are given in Table 7.

### HEAT OF RESPIRATION

All living food products respire. During the respiration process, sugar and oxygen are combined to form  $\text{CO}_2$ ,  $\text{H}_2\text{O}$ , and heat as follows:

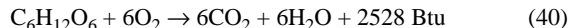
Table 7 Thermal Diffusivity of Foods

Food Item	Thermal Diffusivity, Centistokes	Water Content, % by mass	Fat Content, % by mass	Apparent Density, lb/ft <sup>3</sup>	Temperature, °F	Reference
<b>Fruits and Vegetables</b>						
Apple, Red Delicious, whole <sup>a</sup>	0.14	85	—	52.4	32 to 86	Bennett et al. (1969)
Apple, dried	0.096	42	—	53.4	73	Sweat (1985)
Applesauce	0.11	37	—	—	41	Riedel (1969)
	0.11	37	—	—	149	Riedel (1969)
	0.12	80	—	—	41	Riedel (1969)
	0.14	80	—	—	149	Riedel (1969)
Apricots, dried	0.11	44	—	82.6	73	Sweat (1985)
Bananas, flesh	0.12	76	—	—	41	Riedel (1969)
	0.14	76	—	—	149	Riedel (1969)
Cherries, flesh <sup>b</sup>	0.13	—	—	65.5	32 to 86	Parker and Stout (1967)
Dates	0.10	35	—	82.3	73	Sweat (1985)
Figs	0.096	40	—	77.4	73	Sweat (1985)
Jam, strawberry	0.12	41	—	81.7	68	Sweat (1985)
Jelly, grape	0.12	42	—	82.4	68	Sweat (1985)
Peaches <sup>b</sup>	0.14	—	—	59.9	36 to 90	Bennett (1963)
Peaches, dried	0.12	43	—	78.6	73	Sweat (1985)
Potatoes, whole	0.13	—	—	65 to 67	32 to 158	Minh et al. (1969)
						Mathews and Hall (1968)
Potatoes, mashed, cooked	0.12	78	—	—	41	Riedel (1969)
	0.15	78	—	—	149	Riedel (1969)
Prunes	0.12	43	—	76.1	73	Sweat (1985)
Raisins	0.11	32	—	86.1	73	Sweat (1985)
Strawberries, flesh	0.13	92	—	—	41	Riedel (1969)
Sugar beets	0.13	—	—	—	32 to 140	Slavicek (1962)
<b>Meats</b>						
Codfish	0.12	81	—	—	41	Riedel (1969)
	0.14	81	—	—	149	Riedel (1969)
Halibut <sup>c</sup>	0.15	76	1	66.8	104 to 149	Dickerson and Read (1975)
Beef, chuck <sup>d</sup>	0.12	66	16	66.2	104 to 149	Dickerson and Read (1975)
Beef, round <sup>d</sup>	0.13	71	4	68.0	104 to 149	Dickerson and Read (1975)
Beef, tongue <sup>d</sup>	0.13	68	13	66.2	104 to 149	Dickerson and Read (1975)
Beefstick	0.11	37	—	65.5	68	Sweat (1985)
Bologna	0.13	65	—	62.4	68	Sweat (1985)
Corned beef	0.11	65	—	—	41	Riedel (1969)
	0.13	65	—	—	149	Riedel (1969)
Ham, country	0.14	72	—	64.3	68	Sweat (1985)
Ham, smoked	0.12	64	—	—	41	Riedel (1969)
Ham, smoked <sup>d</sup>	0.13	64	14	68.0	104 to 149	Dickerson and Read (1975)
Pepperoni	0.093	32	—	66.1	68	Sweat (1985)
Salami	0.13	36	—	59.9	68	Sweat (1985)
<b>Cakes</b>						
Angel food	0.26	36	—	9.2	73	Sweat (1985)
Applesauce	0.12	24	—	18.7	73	Sweat (1985)
Carrot	0.12	22	—	20.0	73	Sweat (1985)
Chocolate	0.12	32	—	21.2	73	Sweat (1985)
Pound	0.12	23	—	30.0	73	Sweat (1985)
Yellow	0.12	25	—	18.7	73	Sweat (1985)
White	0.10	32	—	27.8	73	Sweat (1985)

<sup>a</sup>Data are applicable only to raw whole apple.<sup>c</sup>Stored frozen and thawed prior to test.<sup>b</sup>Freshly harvested.<sup>d</sup>Data are applicable only where the juices exuded during heating remain in the food samples.

Table 8 Commodity Respiration Coefficients (Becker et al. 1996b)

Commodity	Respiration Coefficients		Commodity	Respiration Coefficients	
	<i>f</i>	<i>g</i>		<i>f</i>	<i>g</i>
Apples	$5.6871 \times 10^{-4}$	2.5977	Onions	$3.668 \times 10^{-4}$	2.538
Blueberries	$7.2520 \times 10^{-5}$	3.2584	Oranges	$2.8050 \times 10^{-4}$	2.6840
Brussels sprouts	0.0027238	2.5728	Peaches	$1.2996 \times 10^{-5}$	3.6417
Cabbage	$6.0803 \times 10^{-4}$	2.6183	Pears	$6.3614 \times 10^{-5}$	3.2037
Carrots	0.050018	1.7926	Plums	$8.608 \times 10^{-5}$	2.972
Grapefruit	0.0035828	1.9982	Potatoes	0.01709	1.769
Grapes	$7.056 \times 10^{-5}$	3.033	Rutabagas (swedes)	$1.6524 \times 10^{-4}$	2.9039
Green peppers	$3.5104 \times 10^{-4}$	2.7414	Snap beans	0.0032828	2.5077
Lemons	0.011192	1.7740	Sugar beets	$8.5913 \times 10^{-3}$	1.8880
Lima beans	$9.1051 \times 10^{-4}$	2.8480	Strawberries	$3.6683 \times 10^{-4}$	3.0330
Limes	$2.9834 \times 10^{-8}$	4.7329	Tomatoes	$2.0074 \times 10^{-4}$	2.8350



In most stored plant products, little cell development takes place, and the greater part of respiration energy is released in the form of heat, which must be taken into account when cooling and storing these living commodities (Becker et al. 1996a). The rate at which this chemical reaction takes place varies with the type and temperature of the commodity.

Becker et al. (1996b) developed correlations that relate a commodity's rate of carbon dioxide production to its temperature. The carbon dioxide production rate can then be related to the commodity's heat generation rate due to respiration. The resulting correlation gives the commodity's respiratory heat generation rate  $W$  in Btu/h·lb as a function of temperature  $t$  in °F:

$$W = 0.00460f(t)^g \quad (41)$$

The respiration coefficients  $f$  and  $g$  for various commodities are given in Table 8.

Fruits, vegetables, flowers, bulbs, florists' greens, and nursery stock are storage commodities with significant heats of respiration. Dry plant products, such as seeds and nuts, have very low respiration rates. Young, actively growing tissues, such as asparagus, broccoli and spinach, have high rates of respiration as do immature seeds such as green peas and sweet corn. Fast developing fruits such as strawberries, raspberries, and blackberries, have much higher respiration rates than do fruits that are slow to develop, such as apples, grapes, and citrus fruits.

In general, most vegetables, other than root crops, have a high initial respiration rate for the first one or two days after harvest. Within a few days, the respiration rate quickly lowers to the equilibrium rate (Ryall and Lipton 1972).

Fruits, however, are different from most vegetables. Those fruits that do not ripen during storage, such as citrus fruits and grapes, have fairly constant rates of respiration. Those that ripen in storage, such as apples, peaches, and avocados, exhibit an increase in the respiration rate. At low storage temperatures, around 32°F, the rate of respiration rarely increases because no ripening takes place. However, if fruits are stored at higher temperatures (50°F to 60°F), the respiration rate increases due to ripening and then decreases. Soft fruits, such as blueberries, figs, and strawberries, show a decrease in respiration with time at 32°F. If they become infected with decay organisms, however, respiration increases.

Table 9 lists the heats of respiration as a function of temperature for a variety of commodities while Table 10 shows the change in respiration rate with time. Most of the commodities in Table 9 have a low and a high value for heat of respiration at each temperature. When no range is given, the value is an average for the specified temperature and may be an average of the respiration rates for many days.

When using Table 9, select the lower value for estimating the heat of respiration at the equilibrium storage state and use the higher value for calculating the heat load for the first day or two after harvest, including precooling and short-distance transport. During the storage of fruits between 32°F and 40°F, the increase in the respiration rate due to ripening is slight. However, for fruits, such as mangoes, avocados, or bananas, stored at temperatures above 50°F, significant ripening occurs and the higher rates listed in Table 9 should be used. Vegetables, such as onions, garlic, and cabbage, can exhibit an increase in heat production after a long storage period.

### TRANSPIRATION OF FRESH FRUITS AND VEGETABLES

The most abundant constituent in fresh fruits and vegetables is water, which exists as a continuous liquid phase within the fruit or

vegetable. Transpiration is the process by which fresh fruits and vegetables lose some of this water. This process consists of the transport of moisture through the skin of the commodity, the evaporation of this moisture from the commodity surface, and the convective mass transport of the moisture to the surroundings (Becker et al. 1996b).

The rate of transpiration in fresh fruits and vegetables affects product quality. Moisture transpires continuously from commodities during handling and storage. Some moisture loss is inevitable and can be tolerated. However, under many conditions, the loss of moisture may be sufficient to cause the commodity to shrivel. The resulting loss in mass not only affects appearance, texture, and flavor of the commodity, but also reduces the salable mass (Becker et al. 1996a).

Many factors affect the rate of transpiration from fresh fruits and vegetables. Moisture loss from a fruit or vegetable is driven by a difference in water vapor pressure between the product surface and the environment. Becker and Fricke (1996a) state that the product surface may be assumed to be saturated, and thus, the water vapor pressure at the commodity surface is equal to the water vapor saturation pressure evaluated at the product's surface temperature. However, they also report that dissolved substances in the moisture of the commodity tend to lower the vapor pressure at the evaporating surface slightly.

Evaporation that occurs at the product surface is an endothermic process that cools the surface, thus lowering the vapor pressure at the surface and reducing transpiration. Respiration within the fruit or vegetable, on the other hand, tends to increase the product's temperature, thus raising the vapor pressure at the surface and increasing transpiration. Furthermore, the respiration rate is itself a function of the commodity's temperature (Gaffney et al. 1985). In addition, factors such as surface structure, skin permeability, and air flow also effect the transpiration rate (Sastry et al. 1978).

Becker et al. (1996c) performed a numerical, parametric study to investigate the influence of bulk mass, air flow rate, skin mass transfer coefficient, and relative humidity on the cooling time and moisture loss of a bulk load of apples. They found that relative humidity and skin mass transfer coefficient had little effect on cooling time while bulk mass and airflow rate were of primary importance to cooling time. Moisture loss was found to vary appreciably with relative humidity, airflow rate, and skin mass transfer coefficient while bulk mass had little effect. They reported that an increase in airflow results in a decrease in moisture loss. The increased airflow reduces the cooling time, which quickly reduces the vapor pressure deficit, thus lowering the transpiration rate.

The driving force for transpiration is a difference in water vapor pressure between the surface of a commodity and the surrounding air. Thus, the basic form of the transpiration model is as follows:

$$\dot{m} = k_t(p_s - p_a) \quad (42)$$

where  $\dot{m}$  is the transpiration rate expressed as the mass of moisture transpired per unit area of commodity surface per unit time. This rate may also be expressed per unit mass of commodity rather than per unit area of commodity surface. The transpiration coefficient  $k_t$  is the mass of moisture transpired per unit area of commodity, per unit water vapor pressure deficit, per unit time. The transpiration coefficient may also be expressed per unit mass of commodity rather than per unit area of commodity surface. The quantity  $(p_s - p_a)$  is the water vapor pressure deficit. The water vapor pressure at the commodity surface  $p_s$  is the water vapor saturation pressure evaluated at the commodity surface temperature while the water vapor pressure in the surrounding air  $p_a$  is a function of the relative humidity of the air.

In its simplest form, the transpiration coefficient  $k_t$  is considered to be a constant for a particular commodity. Table 11 lists

Table 9 Heat of Respiration of Fresh Fruits and Vegetables Held at Various Temperatures

Commodity	Heat of Respiration, Btu/day per Ton of Produce						Reference
	32°F	41°F	50°F	59°F	68°F	77°F	
<b>Apples</b>							
Yellow, transparent	1513	2665	—	7889	12,392	—	Wright et al. (1954)
Delicious	757	1117	—	—	—	—	Lutz and Hardenburg (1968)
Golden Delicious	793	1189	—	—	—	—	Lutz and Hardenburg (1968)
Jonathan	865	1295	—	—	—	—	Lutz and Hardenburg (1968)
McIntosh	793	1189	—	—	—	—	Lutz and Hardenburg (1968)
Early cultivars	720-1369	1153-2342	3062-4503	3962-6844	4323-9005	—	IIR (1967)
Late cultivars	396-793	1008-1549	1513-2306	2053-4323	3242-5403	—	IIR (1967)
Average of many cultivars	505-901	1117-1585	—	2990-6808	3711-7709	—	Lutz and Hardenburg (1968)
Apricots	1153-1261	1405-1982	2449-4143	4683-7565	6484-11,527	—	Lutz and Hardenburg (1968)
Artichokes, Globe	5007-9907	7025-13,220	1203-21,649	1704-31,951	3004-51,403	—	Sastry et al. (1978), Rappaport and Watada (1958)
Asparagus	6015-17,651	12,032-30,043	23,630-67,146	35,086-72,152	60,121-110,228	—	Sastry et al. (1978), Lipton (1957)
Avocados	*b	*b	—	13,61634,581	16,246-76,439	—	Lutz and Hardenburg (1968), Biale (1960)
Bananas, green	*b	*b	†b	4431-7626	6484-11,527	—	IIR (1967)
Bananas, ripening	*b	*b	†b	6484-9726	7204-18,011	—	IIR (1967)
<b>Beans</b>							
Lima, unshelled	2306-6628	4323-7925	—	22,046-27,449	29,250-39,480	—	Lutz and Hardenburg (1968), Tewfik and Scott (1954)
Lima, shelled	3890-7709	6412-13,436	—	—	46,577-59,509	—	Lutz and Hardenburg (1968), Tewfik and Scott (1954)
Snap	*b	7529-7709	12,032-12,824	18,731-20,533	26,044-28,673	—	Ryall and Lipton (1972), Watada and Morris (1966)
Beets, red, roots	1189-1585	2017-2089	2594-2990	3711-5115	—	—	Ryall and Lipton (1972), Smith (1957)
<b>Berries</b>							
Blackberries	3458-5043	6304-10,086	11,527-20,893	15,489-32,060	28,818-43,227	—	IIR (1967)
Blueberries	505-2306	2017-2702	—	7529-13,616	11,419-19,236	—	Lutz and Hardenburg (1968)
Cranberries	*b	901-1008	—	—	2413-3999	—	Lutz and Hardenburg (1968) Anderson et al. (1963)
Gooseberries	1513-1909	2702-2990	—	4791-7096	—	—	Lutz and Hardenburg (1968), Smith (1966)
Raspberries	3890-5512	6808-8501	6124-12,248	18,119-22,334	25,215-54,033	—	Lutz and Hardenburg (1968), IIR (1967), Haller et al. (1941)
Strawberries	2702-3890	3602-7313	10,807-20,893	15,634-20,317	22,514-43,154	37,247-46,468	Lutz and Hardenburg (1968), IIR (1967), Maxie et al. (1959)
Broccoli, sprouting	4107-4719	7601-35,226	—	38,256-74,890	61,274-75,106	85,805-123,376	Lutz and Hardenburg (1968), Morris (1947), Scholz et al. (1963)
Brussels Sprouts	3386-5295	7096-10,698	13,904-18,623	21,037-23,523	19,848-41,894	—	Sastry et al. (1978), Smith (1957)
<b>Cabbage</b>							
Penn State	865	2089-2234	—	4935-6988	—	—	Van den Berg and Lentz (1972)
White, winter	1081-1801	1621-3062	2702-3962	4323-5944	7925-9006	—	IIR (1967)
White, spring	2089-2990	3890-4719	6412-7313	11,815-12,609	—	—	Sastry et al. (1978), Smith (1957)
Red, early	1693-2161	3423-3783	5224-61,238	8105-9366	12,248-12,608	—	IIR (1967)
Savoy	3422-4683	5584-6484	11,527-13,509	19,272-21,794	28,818-32,420	—	IIR (1967)
<b>Carrots, Roots</b>							
Imperator, Texas	3386	4323	6916	8718	15,526	—	Scholz et al. (1963) Smith(1957)
Main Crop, U.K.	757-1513	1296-2666	2161-3423	6448-14,589 at 65°F	—	—	—
Nantes, Canada <sup>d</sup>	684	1477	—	4755-6232	—	—	Van den Berg and Lentz (1972)
Cauliflower, Texas	3926	4503	7456	10,158	17,687	—	Scholz et al. (1963)
Cauliflower, U.K.	1693-5295	4323-6015	9006-10,734	14,841-18,047	—	—	Smith (1957)
Celery, N.Y., white	1585	2413	—	8215	14,229	—	Lutz and Hardenburg (1968)
Celery, U.K.	1117-1585	2017-2810	4323-6015	8609-9221 at 65°F	—	—	Smith(1957)
Celery, Utah, Canada <sup>e</sup>	1117	1982	—	6556	—	—	Van den Berg and Lentz (1972)
Cherries, sour	296-2918	2810-2918	—	6015-11,022	8609-11,022	11,708-15,634	Lutz and Hardenburg (1968), Hawkins (1929)

**Table 9 Heat of Respiration of Fresh Fruits and Vegetables Held at Various Temperatures (Continued)**

Commodity	Heat of Respiration, Btu/day per Ton of Produce						Reference
	32°F	41°F	50°F	59°F	68°F	77°F	
Cherries, sweet	901-1189	2089-3098	—	5512-9907	6196-7025	—	Lutz and Hardenburg (1968), Micke et al. (1965)
Corn, sweet with husk, Texas	9366	17,111	24,676	35,878	63,543	89,695	Scholz et al. (1963)
Cucumbers, Calif.	*b	*b	5079-6376	5295-7313	6844-10,591	—	Eaks and Morris (1956)
Figs, mission	—	2413-2918	4863-5079	10,807-13,940	12,536-20,929	18,731-20,929	Lutz and Hardenburg (1968), Claypool and Ozbek (1952)
Garlic	648-2413	1296-2125	2017-2125	2413-6015	2197-3999	—	Suistry et al. (1978), Mann and Lewis (1956)
<b>Grapes</b>							
Concord	612	1189	—	3494	7204	8501	Lutz and Hardenburg (1968), Lutz (1938)
Emperor	288-505	684-1296	1801	2197-2594	—	5512-6628	Lutz and Hardenburg (1968), Pentzer et al. (1933)
Thompson seedless	432	1045	1693	—	—	—	Wright et al. (1954)
Ohanez	288	720	2	—	—	—	Wright et al. (1954)
Grapefruit, Calif. Marsh	*b	*b	*b	2594	3890	4791	Haller et al. (1945)
Grapefruit, Florida	*b	b	*b	2810	3494	4214	Haller et al. (1945)
Horseradish	1801	2377	5800	7204	9834	—	Sastry et al. (1978)
Kiwi fruit	616	1455	2889	—	3858-4254	—	Saravacos and Pilsworth (1965)
Kohlrabi	2197	3602	6916	10,807	—	—	Sastry et al. (1978)
Leeks	2089-3062	4323-6412	11,815-15,021	18,227-25,756	—	—	Sastry et al. (1978), Smith (1957)
Lemons, Calif., Eureka	*b	*b	*b	3494	5007	5727	Haller (1945)
<b>Lettuce</b>							
Head, Calif.	2017-3711	2918-4395	6015-8826	8501-9006	13,220	—	Sastry et al. (1978)
Head, Texas	2306	2918	4791	7925	12,536	181 at 180°F	Watt and Merrill (1963), Lutz and Hardenburg, (1968)
Leaf, Texas	5079	6448	8681	13,869	22,118	32,275	Scholz et al. (1963)
Romaine, Texas	—	4575	7817	9762	15,093	23,883	Scholz et al. (1963)
Limes, Persian	*b	*b	576-1261	1296-2306	1513-4107	3314-10,014	Lutz and Hardenburg (1968)
Mangos	*b	*b	—	9907	16,534-33,356	26,441	Lutz and Hardenburg (1968), Gore (1911), Karmarkar and Joshe (1941)
<b>Melons</b>							
Cantaloupes	*b	1909-2197	3423	7420-8501	9834-14,229	13,725-15,741	Lutz and Hardenburg (1968), Sastry et al. (1978), Scholz et al. (1963)
Honeydew	—	*b	1765	2594-3494	4395-5259	5800-7601	Lutz and Hardenburg (1968), Scholz (1963), Pratt and Morris (1958)
Watermelon	*b	*b	1657	—	3818-5512	—	Lutz and Hardenburg (1968), Scholz et al. (1963)
Mint <sup>m</sup>	1769-3306	6614	16,754-20,061	23,148-29,981	36,595-50,041	56,655-69,883	Hruschka and Want (1979)
Mushrooms	6196-9618	15,634	—	—	58,104-69,738	—	Lutz and Hardenburg (1968), Smith (1964)
Nuts (kind not specified)	181	360	720	720	1081	—	IIR (1967)
Okra, Clemson	*b	76,043	19,236	32,132	57,527	76,040 at 85°F	Scholz et al. (1963)
<b>Onions</b>							
Dry, Autumn Spice <sup>f</sup>	505-684	793-1477	—	2089-5548	—	—	Van den Berg and Lentz (1972)
Dry, White Bermuda	648	757	1585	2449	3711	6196 at 80°F	Scholz et al. (1963)
Green, N.J.	2306-4899	3819-15,021	7961-12,968	14,553-21,434	17,205-34,225	21,541-46,217	Lutz and Hardenburg (1968)
Olives, Manzanillo	*b	*b	—	4791-8609	8501-10,807	9006-13,436	Maxie et al. (1959)
Oranges, Florida	684	1405	2702	4611	6628	7817 at 80°F	Haller (1945)
Oranges, Calif., W. Navel	*b	1405	2990	5007	6015	7997	Haller (1945)
Oranges, Calif., Valencia	*b	1008	2594	2810	3890	4611	Haller (1945)
Papayas	*b	*b	2485	3314-4791	—	8609-21,613	Pantastico (1974), Jones (1942)
Parsley <sup>m</sup>	7277-10,140	14,549-18,738	28,879-36,155	31,746-49,163	43,208-56,216	67,902-75,174	Hruschka and Want (1979)
Parsnips, U.K.	2558-3423	1946-3854	4503-5800	7096-9438	—	—	Smith (1957)
Parsnips Hollow Crown, Canada	793-1801	1369-3386	—	4755-10,195	—	—	Van den Berg and Lentz (1972)

Table 9 Heat of Respiration of Fresh Fruits and Vegetables Held at Various Temperatures (Continued)

Commodity	Heat of Respiration, Btu/day per Ton of Produce						Reference
	32 °F	41 °F	50 °F	59 °F	68 °F	77 °F	
Peaches, Elberta	829	1441	3458	7565	13,509	19,812 at 80 °F	Haller et al. (1932)
Peaches, several cultivars	901-1405	1405-2017	—	7313-9330	13,040-22,549	17,939-26,837	Lutz and Hardenburg (1968)
<b>Peanuts</b>							
Cured <sup>h</sup>	3 at 85 °F					51 at 85 °F	Thompson et al. (1951)
Not cured, VA Bunch <sup>i</sup>						3120 at 85 °F	Schenk (1959, 1961)
Dixie Spanish						1823 at 85 °F	Schenk (1959, 1961)
<b>Pears</b>							
Bartlett	684-1513	1117-2197	—	3314-13,220	6628-15,417	—	Lutz and Hardenburg (1968)
late ripening	576-793	1296-3062	1729-4143	6124-9366	7204-16,210	—	IIR (1967)
early ripening	576-1081	1621-3423	2161-4683	7565-11,887	8645-19,812	—	IIR (1967)
Peas, green-in-pod	6700-10,302	12,139-16,822	—	39,372-44,595	54,105-79,645	75,646-83,067	Lutz and Hardenburg (1968), Tewfik and Scott (1954)
Peas, shelled	10,410-16,642	17,435-21,444	—	—	76,871-10,893	—	Lutz and Hardenburg (1968), Tewfik and Scott (1954)
Peppers, sweet	* <sup>b</sup>	* <sup>b</sup>	3170	5043	9654	—	Schol et al. (1963)
Persimmons	1296		2594-3098		4395-5295	6412-8826	Lutz and Hardenburg (1968), Gore (1911)
Pineapple, mature green	* <sup>b</sup>	* <sup>b</sup>	1225	2846	5331	7817 at 80 °F	Schol et al. (1963)
Pineapple, ripening	* <sup>b</sup>	* <sup>b</sup>	1657	3999	8790	13,797	Schol et al. (1963)
Plums, Wickson	432-648	865-1982	1981-2522	2630-2737	3962-5727	6160-15,634	Claypool and Allen (1951)
<b>Potatoes</b>							
Calif. White Rose, Immature	* <sup>b</sup>	2594	3098-4611	3098-6808	3999-9932	Sastry et al. (1978)	
Mature	* <sup>b</sup>	1296-1513	1467-2197	1467-2594	1467-3494	Sastry et al. (1978)	
Very mature	* <sup>b</sup>	1117-1513	1513	1513-2197	2017-2630	Sastry et al. (1978)	
Katahdin, Canada <sup>j</sup>	* <sup>b</sup>	865-936	1729-2234		Van den Berg and Lentz (1972)		
Kennebec	* <sup>b</sup>	793-936	936-1982		Van den Berg and Lentz (1972)		
Radishes, with tops	3206-3818	4214-4611	6808-8105	15,417-17,146	27,341-30,043	34,869-42,470	Lutz and Hardenburg (1968)
Radishes, topped	1189-1296	1693-1801	3314-3494	6124-7204	10,519-10,807	14,841-16,751	Lutz and Hardenburg (1968)
Rhubarb, topped	1801-2918	2413-3999	6808-10,014		8826-12,536	Hruschka (1966)	
Rutabaga, Laurentian, Can. <sup>k</sup>	432-612	1045-1124	2342-3458		Van den Berg and Lentz (1972)		
<b>Spinach</b>							
Texas	10,122		24,387	39,409	50,683	Schol et al. (1963)	
U.K., summer	2558-4719	6015-7096	12,896-16,534	40,777-47,65 at 65 °F		Smith (1957)	
U.K., winter	3854-5584	6448-13,869	15,021-22,766	42,938-53,673 at 65 °F		Smith (1957)	
<b>Squash</b>							
Summer, yellow, straight-neck	† <sup>b</sup>	† <sup>b</sup>	7709-8105	16,534-20,028	18,731-21,434	Lutz and Hardenburg (1968)	
Winter Butternut	* <sup>b</sup>	* <sup>b</sup>			16,318-26,908	Lutz and Hardenburg (1968)	
<b>Sweet Potatoes</b>							
Cured, Puerto Rico	* <sup>b</sup>	* <sup>b</sup>	† <sup>b</sup>	3530-4863	Lewis and Morris (1956)		
Cured, Yellow Jersey	* <sup>b</sup>	* <sup>b</sup>	† <sup>b</sup>	4863-5079	Lewis and Morris (1956)		
Noncured	* <sup>b</sup>	* <sup>b</sup>	* <sup>b</sup>	6304	11,923-16,138	Lutz and Hardenburg (1968)	
<b>Tomatoes</b>							
Texas, mature green	* <sup>b</sup>	* <sup>b</sup>	* <sup>b</sup>	4503	7637	9402 at 80 °F	Schol et al. (1963)
Texas, ripening	* <sup>b</sup>	* <sup>b</sup>	* <sup>b</sup>	5872	8933	10,627 at 80 °F	Schol et al. (1963)
Calif. mature green	* <sup>b</sup>	* <sup>b</sup>	* <sup>b</sup>	5295-7709		6592-10,591	Workman and Pratt (1957)
Turnip, roots	1909	2089-2197	4719-5295		5295-5512	Lutz and Hardenburg (1968)	
Watercress <sup>l</sup>	3306	9920	20,061-26,674	29,981-43,208	66,576-76,719	76,720-96,561	Hruschka and Want (1979)

<sup>a</sup>Column headings indicate temperatures at which respiration rates were determined, within 2 °F, except where the actual temperatures are given.

<sup>b</sup>The symbol \* denotes a chilling temperature. The symbol † denotes the temperature is borderline, not damaging to some cultivars, if exposure is short.

<sup>c</sup>Rates are for 30 to 60 days and 60 to 120 days storage, the longer storage having the higher rate, except at 32 °F, where they were the same.

<sup>d</sup>Rates are for 30 to 60 days and 120 to 180 days storage, respiration increasing with time only at 59 °F.

<sup>e</sup>Rates are for 30 to 60 days storage.

<sup>f</sup>Rates are for 30 to 60 days and 120 to 180 days storage; rates increased with time at all temperatures as dormancy was lost.

<sup>g</sup>Rates are for 30 to 60 days and 120 to 180 days; rates increased with time at all temperatures.

<sup>h</sup>Shelled peanuts with about 7% moisture. Respiration after 60 h curing was almost negligible, even at 85 °F.

<sup>i</sup>Respiration for freshly dug peanuts, not cured, with about 35 to 40% moisture. During curing, peanuts in the shell were dried to about 5 to 6% moisture, and in roasting are dried further to about 2% moisture.

<sup>j</sup>Harvested 141 days after planting (Morris 1952).

<sup>k</sup>Rates are for 30 to 60 days and 120 to 180 days with rate declining with time at 41 °F but increasing at 59 °F as sprouting started.

<sup>l</sup>Rates are for 30 to 60 days and 120 to 180 days; rates increased with time, especially at 59 °F where sprouting occurred.

<sup>m</sup>Rates are for 1 day after harvest.

Table 10 Change in Respiration Rates with Time

Commodity	Days in Storage	Heat of Respiration, Btu/day per Ton of Produce		Reference	Commodity	Days in Storage	Heat of Respiration, Btu/day per Ton of Produce		Reference	
		32°F	41°F				32°F	41°F		
Apples, Grimes	7	648	2882	Harding (1929)	Garlic	10	865	1982	Mann and Lewis (1956)	
			at 50°F			30	1333	3314		
	30	648	3854			180	3098	7277		
Artichokes, Globe	1	9907	13,220	Rappaport and Watada (1958)	Lettuce, Great Lakes	1	3747	4395	Pratt et al. (1954)	
	4	5512	7709			5	1982	33		
	16	3314	5727			10	1765	3314		
Asparagus, Martha Washington	1	17,652	2316	Lipton (1957)	Olives, Manzanillo	1	—	8610	Maxie et al. (1960)	
	3	8682	14,337			at 60°F	5	—		6376
	16	6160	6629			10	—	4864		
Beans, lima, in pod	2	6593	7925	Tewfik and Scott (1954)	Onions, red	1	360	—	Karmarkar and Joshe (1941)	
	4	4431	6376			30	541	—		
	6	3890	5836			120	720	—		
Blueberries, Blue Crop	1	1585	—	Claypool and Allen (1951)	Plums, Wickson	2	432	865	Claypool and Allen (1951)	
	2	584	—			6	432	1549		
		1261	—			18	648	1982		
Broccoli, Waltham 29	1	—	16,102	Morris (1959)	Potatoes	2	—	1333	Morris (1959)	
	4	—	9690			6	—	1765		
	8	—	7277			10	—	1549		
Corn, sweet, in husk	1	11,312	—	Scholz et al. (1963)	Strawberries, Shasta	1	3873	6305	Maxie et al. (1959)	
	2	8106	—			2	2918	6772		
	4	6772	—			5	2918	7277		
Figs, Mission	1	2882	—	Claypool and Ozbek (1952)	Tomatoes, Pearson, mature green	5	—	706	Workman and Pratt (1957)	
	2	2630	—			at 70°F	15	—		6160
	12	2630	—			20	—	5295		

values for the transpiration coefficients  $k_t$  of various fruits and vegetables (Sastry et al. 1978). Because of the many factors that influence transpiration rate, not all the values in Table 11 are reliable. They are to be used primarily as a guide or as a comparative indication of various commodity transpiration rates obtained from the literature.

Fockens and Meffert (1972) modified the simple transpiration coefficient to model variable skin permeability and to account for air flow rate. Their modified transpiration coefficient takes the following form:

$$k_t = \frac{1}{\frac{1}{k_a} + \frac{1}{k_s}} \quad (43)$$

where  $k_a$  is the air film mass transfer coefficient and  $k_s$  is the skin mass transfer coefficient. The air film mass transfer coefficient  $k_a$  describes the convective mass transfer which occurs at the surface of the commodity and is a function of air flow rate. The skin mass transfer coefficient  $k_s$  describes the skin's diffusional resistance to moisture migration.

The air film mass transfer coefficient  $k_a$  can be estimated by using the Sherwood-Reynolds-Schmidt correlations (Becker et al. 1996b). The Sherwood number is defined as follows:

$$Sh = \frac{k_a' d}{\delta} \quad (44)$$

where  $k_a'$  is the air film mass transfer coefficient,  $d$  is the diameter of the commodity, and  $\delta$  is the coefficient of diffusion of water vapor in air. For convective mass transfer from a spherical fruit or vegetable, Becker and Fricke (1996b) recommend the following Sherwood-Reynolds-Schmidt correlation, which was taken from Geankoplis (1978):

$$Sh = 2.0 + 0.552Re^{0.53}Sc^{0.33} \quad (45)$$

In the equation  $Re$  is the Reynolds number ( $Re = u d/\nu$ ) and  $Sc$  is the Schmidt number ( $Sc = \nu/\delta$ ) where  $u$  is the free stream air velocity and  $\nu$  is the kinematic viscosity of air. The driving force for  $k_a'$  is concentration. However, the driving force in the transpiration model is vapor pressure. Thus, the following conversion from concentration to vapor pressure is required:

Table 11 Transpiration Coefficients of Certain Fruits and Vegetables

Commodity and Variety	Transpiration Coefficient, ppm/(h·in.Hg)	Commodity and Variety	Transpiration Coefficient, ppm/(h·in.Hg)	Commodity and Variety	Transpiration Coefficient, ppm/(h·in.Hg)
<b>Apples</b>		<b>Leeks</b>		<b>Pears</b>	
Jonathan	430	Musselburgh	12,600	Passe Crane	974
Golden Delicious	710	<i>Average for all varieties</i>	<b>9600</b>	Beurre Clairgeau	986
Bramley's Seedling	510	<b>Lemons</b>		<i>Average for all varieties</i>	<b>840</b>
<i>Average for all varieties</i>	<b>510</b>	Eureka		<b>Plums</b>	
<b>Brussels Sprouts</b>		Dark green	2760	Victoria	
Unspecified	40,100	Yellow	1700	Unripe	2410
<i>Average for all varieties</i>	<b>75,000</b>	<i>Average for all varieties</i>	<b>2270</b>	Ripe	1400
<b>Cabbage</b>		<b>Lettuce</b>		Wickson	1510
Penn State Ballhead		Unrivalled	106,000	<i>Average for all varieties</i>	<b>1660</b>
Trimmed	3300	<i>Average for all varieties</i>	<b>90,200</b>	<b>Potatoes</b>	
Untrimmed	4920	<b>Onions</b>		Manona	
Mammoth		Autumn Spice		Mature	304
Trimmed	2920	Uncured	1170	Kennebec	
<i>Average for all varieties</i>	<b>2720</b>	Cured	535	Uncured	2080
<b>Carrots</b>		Sweet White Spanish		Cured	730
Nantes	20,000	Cured	1500	Sebago	
Chantenay	21,500	<i>Average for all varieties</i>	<b>730</b>	Uncured	1920
<i>Average for all varieties</i>	<b>14,700</b>	<b>Oranges</b>		Cured	462
<b>Celery</b>		Valencia	710	<i>Average for all varieties</i>	<b>540</b>
Unspecified varieties	25,400	Navel	1270	<b>Rutabagas</b>	
<i>Average for all varieties</i>	<b>21,500</b>	<i>Average for all varieties</i>	<b>1430</b>	Laurentian	5710
<b>Grapefruit</b>		<b>Parsnips</b>		<b>Tomatoes</b>	
Unspecified varieties	380	Hollow Crown	23,500	Marglobe	864
March	670	<b>Peaches</b>		Eurocross BB	1410
<i>Average for all varieties</i>	<b>990</b>	Redhaven		<i>Average for all varieties</i>	<b>1710</b>
<b>Grapes</b>		Hard mature	11,200		
Emperor	960	Soft mature	12,400		
Cardinal	1220	Elberta	3330		
Thompson	2480	<i>Average for all varieties</i>	<b>6970</b>		
<i>Average for all varieties</i>	<b>1500</b>				

Note: Sastry et al. (1978) gathered this data as part of a literature review. The averages reported are the average of all published data found by Sastry et al. for each commodity. Sastry et al. selected specific varietal data because they considered it to be highly reliable data.

$$k_a = \frac{1}{R_{H_2O} T} k_a' \quad (46)$$

where  $R_{H_2O}$  is the gas constant for water vapor and  $T$  is the absolute mean temperature of the boundary layer.

The skin mass transfer coefficient  $k_s$ , which describes the resistance to moisture migration through the skin of a commodity, is based upon the fraction of the product surface covered by pores. Although it is difficult to theoretically determine the skin mass transfer coefficient, experimental determination has been performed by Chau et al. (1987) and Gan and Woods (1989). These experimental values of  $k_s$  are given in Table 12, along with estimated values of the skin mass transfer coefficient for grapes, onions, plums, and potatoes. Note that three values of skin mass transfer coefficient are tabulated for most commodities. These values correspond to the spread of the experimental data.

### SURFACE HEAT TRANSFER COEFFICIENT

Although the surface heat transfer coefficient is not a thermal property of a food or beverage, it is needed to design heat transfer equipment for the processing of foods and beverages where convection is involved. Newton's law of cooling defines the surface heat transfer coefficient  $h$  as follows:

$$q = hA(t_s - t) \quad (47)$$

Table 12 Commodity Skin Mass Transfer Coefficient

Commodity	Skin Mass Transfer Coefficient, $k_s$ , lb/(ft <sup>2</sup> ·h·in.Hg)			Standard Deviation
	Low	Mean	High	
Apples	$2.77 \times 10^{-4}$	$4.17 \times 10^{-4}$	$5.67 \times 10^{-4}$	$7.49 \times 10^{-5}$
Blueberries	$2.38 \times 10^{-3}$	$5.47 \times 10^{-3}$	$8.46 \times 10^{-3}$	$1.60 \times 10^{-3}$
Brussels sprouts	$2.41 \times 10^{-2}$	$3.32 \times 10^{-2}$	$4.64 \times 10^{-2}$	$6.09 \times 10^{-3}$
Cabbage	$6.24 \times 10^{-3}$	$1.68 \times 10^{-2}$	$3.25 \times 10^{-2}$	$7.09 \times 10^{-3}$
Carrots	$7.94 \times 10^{-2}$	$3.90 \times 10^{-1}$	$9.01 \times 10^{-1}$	$1.90 \times 10^{-1}$
Grapefruit	$2.72 \times 10^{-3}$	$4.19 \times 10^{-3}$	$5.54 \times 10^{-3}$	$8.24 \times 10^{-4}$
Grapes	—	$1.00 \times 10^{-3}$	—	—
Green peppers	$1.36 \times 10^{-3}$	$5.39 \times 10^{-3}$	$1.09 \times 10^{-2}$	$1.77 \times 10^{-3}$
Lemons	$2.72 \times 10^{-3}$	$5.19 \times 10^{-3}$	$8.74 \times 10^{-3}$	$1.60 \times 10^{-3}$
Lima beans	$8.16 \times 10^{-3}$	$1.08 \times 10^{-2}$	$1.43 \times 10^{-2}$	$1.47 \times 10^{-3}$
Limes	$2.60 \times 10^{-3}$	$5.54 \times 10^{-3}$	$8.69 \times 10^{-3}$	$1.40 \times 10^{-3}$
Onions	—	$2.22 \times 10^{-3}$	—	—
Oranges	$3.45 \times 10^{-3}$	$4.29 \times 10^{-3}$	$5.34 \times 10^{-3}$	$5.24 \times 10^{-4}$
Peaches	$3.40 \times 10^{-3}$	$3.55 \times 10^{-2}$	$1.15 \times 10^{-1}$	$1.30 \times 10^{-2}$
Pears	$1.31 \times 10^{-3}$	$1.71 \times 10^{-3}$	$3.00 \times 10^{-3}$	$3.72 \times 10^{-4}$
Plums	—	$3.44 \times 10^{-3}$	—	—
Potatoes	—	$1.59 \times 10^{-3}$	—	—
Rutabagas (swedes)	—	$2.91 \times 10^{-1}$	—	—
Snap beans	$8.64 \times 10^{-3}$	$1.41 \times 10^{-2}$	$2.50 \times 10^{-2}$	$4.42 \times 10^{-3}$
Sugar beets	$2.27 \times 10^{-2}$	$8.39 \times 10^{-2}$	$2.18 \times 10^{-1}$	$5.02 \times 10^{-2}$
Strawberries	$9.86 \times 10^{-3}$	$3.40 \times 10^{-2}$	$6.62 \times 10^{-2}$	$1.20 \times 10^{-2}$
Tomatoes	$5.42 \times 10^{-4}$	$2.75 \times 10^{-3}$	$6.07 \times 10^{-3}$	$1.67 \times 10^{-3}$

Source: Becker and Fricke (1996a)



Table 13 Surface Heat Transfer Coefficients for Food Products

1	2	3	4	5	6	7	8	9	10
Product	Shape Length, in. <sup>a</sup>	Transfer Medium	$\Delta t$ and/or Temp. $t$ of Medium, °F	Velocity of Medium, ft/s	Reynolds Number Range <sup>b</sup>	$h$ , Btu/(h·ft <sup>2</sup> ·°F)	Nu-Re-Pr Correlation <sup>c</sup>	Reference	Comments
Apple, Jonathan	Spherical 2.0	Air	$t = 81$	0	N/A	2.0	N/A	Kopelman et al. (1966)	N/A indicates that data were not reported in original article
				1.3		3.0			
				3.0		4.8			
				6.7		8.0			
				17.0		9.4			
				0		2.0			
	2.3			1.3		3.0			
				3.0		4.9			
				6.7		7.9			
				17.0		9.6			
				0		2.0			
				1.3		2.8			
2.4			3.0		4.6				
			6.7		6.9				
			17.0		8.9				
			0		2.0				
			1.3		2.8				
			3.0		4.6				
Apple, Red Delicious	2.5	Air	$\Delta t = 41$ $t = 31$	4.9	N/A	4.8	N/A	Nicholas et al. (1964)	Thermocouples at center of fruit.
				15.0		10.0			
				4.9		2.5			
	2.8			15.0		6.5			
				0		1.8			
				4.9		4.0			
3.0			9.8		5.8				
			15.0		6.1				
			0.90		16.0				
2.2	Water	$\Delta t = 46$ $t = 32$			14.0				
					9.8				
					9.8				
Beef carcass	142 lb*	Air	$t = -3$	5.9	N/A	3.8	N/A	Fedorov et al. (1972)	*For size indication.
	187 lb*			1.0		1.8			
Cucumbers	Cylinder 1.5	Air	$t = 39$	3.28	N/A	3.2	$Nu = 0.291Re^{0.592}Pr^{0.333}$	Dincer (1994)	Diameter = 38 mm. Length = 160 mm.
				4.10		305			
				4.92		3.8			
				5.74		4.1			
				6.56		4.7			
						4.7			
Eggs, Jifujitori	1.3	Air	$\Delta t = 81$	6.6–26	6000-15000	N/A	$Nu = 0.46Re^{0.56} \pm 1.0\%$	Chuma et al. (1970)	5 points in correlation.
				6.6–26	8000-25000	N/A			
Eggs, leghorn	1.7	Air	$\Delta t = 81$	6.6–26	8000-25000	N/A	$Nu = 0.71Re^{0.55} \pm 1.0\%$	Chuma et al. (1970)	5 points in correlation.
				6.6–26	8000-25000	N/A			
Figs	Spherical 1.85	Air	$t = 39$	3.61	N/A	4.2	$Nu = 1.560Re^{0.426}Pr^{0.333}$	Dincer (1994)	
				4.92		4.6			
				5.74		4.8			
				8.20		5.8			
						5.8			
Fish Pike, perch, sheatfish	N/A	Air	N/A	3.2–22	5000-35000	N/A	$Nu = 4.5Re^{0.28} \pm 10\%$	Khatchaturov (1958)	32 points in correlation.
				3.2–22	5000-35000	N/A			
Grapes	Cylinder 0.43	Air	$t = 39$	3.28	N/A	5.4	$Nu = 0.291Re^{0.592}Pr^{0.333}$	Dincer (1994)	Diameter = 11 mm Length = 22 mm
				4.10		6.0			
				4.92		6.7			
				5.74		7.2			
				6.56		7.4			
						7.4			
Hams, boneless processed	$G^* = 0.4-0.45$ * $G$ = Geometrical factor for shrink-fitted plastic bag	Air	$\Delta t = 132$ $t = 150$	N/A	1000-86000	N/A	$Nu = 0.329Re^{0.564}$	Ref: Clary et al. (1968)	$G = 1/4 + 3/(8A^2) + 3/(8B^2)$ $A = a/Z, B = b/Z$ $A$ = characteristic length = 0.5 min. dist. $\perp$ to airflow $a$ = minor axis $b$ = major axis Correlation on 18 points Recalc with min. distance $\perp$ to airflow Calculated Nu with 1/2 char. length
Hams, processed	N/A	Air	$t = -10$ $t = -55$ $t = -60$ $t = -70$ $t = -80$	2.0	N/A	3.6	N/A	Van den Berg and Lentz (1957)	38 points total. Values are averages.
						3.6			
						3.5			
						3.5			
						3.2			

Table 13 Surface Heat Transfer Coefficients for Food Products (Continued)

1	2	3	4	5	6	7	8	9	10
Product	Shape Length, in. <sup>a</sup>	Transfer Medium	$\Delta t$ and/or Temp. $t$ of Medium, °F	Velocity of Medium, ft/s	Reynolds Number Range <sup>b</sup>	$h$ , Btu/(h·ft <sup>2</sup> ·°F)	Nu-Re-Pr Correlation <sup>c</sup>	Reference	Comments
Meat	Slabs 0.91 thick	Air	$t = 32$	1.8 4.6 12.0	N/A	1.9 3.5 6.2	N/A	Radford et al. (1976)	
Oranges, Grapefruit, Tangelos, bulk packed	Spheroids 2.3 3.1 2.1	Air	$\Delta t = 70$ to 56 $t = 16$	0.36–1.1	35000– 135000	11.7*	$Nu = 5.05Re^{0.333}$	Ref: Bennett et al. (1966)	Bins 42 × 42 × 16 in. 36 points in correlation. Random packaging. Interstitial velocity.
Oranges, Grapefruit, bulk packed	Spheroids 3.0 4.2	Air	$\Delta t = 91$ $t = 32$	0.17–6.7	180– 18000	N/A	$Nu = 1.17Re^{0.529}$	Baird and Gaffney (1976)	20 points in correlation Bed depth: 26 in.
Peas, fluidized bed	Spherical N/A	Air	$t = -15$ to $-35$	4.9–2.4 ±1.0	1000– 4000	N/A	$Nu = 3.5 \times 10^{-4}Re^{1.5}$	Kelly (1965)	Bed depth: 2 in.
Peas, bulk packed	Spherical N/A	Air	$t = -15$ to $-35$	4.9–2.4 ±1.0	1000– 6000	N/A	$Nu = 0.016Re^{0.95}$	Kelly (1965)	
Pears	Spherical 2.36	Air	$t = 39$	3.28 4.10 4.92 5.74 6.56	N/A	2.2 2.5 2.8 2.8 3.4	$Nu = 1.560Re^{0.426}Pr^{0.333}$	Dincer (1994)	
Potatoes Pungo, bulk packed	Ellipsoid N/A N/A	Air	$t = 40$	2.2 4.0 4.5 5.7	3000–9000	2.5* 3.4 3.6 4.3	$Nu = 0.364Re^{0.558}Pr^{1/3}$ (at top of bin)	Ref: Minh et al. (1969)	Use interstitial velocity to calculate Re. Bin is 30 × 20 × 9 in. *Each $h$ value is average of 3 reps with airflow from top to bottom.
Poultry Chickens and turkeys	2.6 to 20.8 lb*	**	$\Delta t = 32$	*	N/A	74 to 83	N/A	Lentz (1969)	Vacuum packaged. * Moderately agitated Chickens 2.4 to 6.4 lb Turkeys 11.9 to 21 lb **CaCl <sub>2</sub> Brine, 26% by mass.
Soybeans	Spherical 2.6	Air	N/A	22	1200– 4600	N/A	$Nu = 1.07Re^{0.64}$	Otten (1974)	8 points in correlation. Bed depth: 1.3 in.
Squash	Cylinder 1.8	Water	1.64 3.28 4.92	0.16	N/A	47.9 36.1 29.2	N/A	Dincer (1993)	Diameter = 1.8 in. Length = 6.1 in.
Tomatoes	Spherical 70	Air	$t = 39$	3.28 4.10 4.92 5.74 6.56	N/A	1.9 2.3 2.4 2.6 3.0	$Nu = 1.560Re^{0.426}Pr^{0.333}$	Dincer (1994)	
Karlsruhe substance	Slab 3.0	Air	$\Delta t = 96$ $t = 100$	N/A	N/A	2.9	N/A	Cleland and Earle (1976)	Packed in aluminum foil and brown paper
Milk container	Cylinder 2.8 × 3.9 2.8 × 5.9 2.8 × 9.8	Air	$\Delta t = 9.5$	N/A	$Gr = 10^6$ – $5 \times 10^7$	N/A	$Nu = 0.754Gr^{0.264}$	Leichter et al. (1976)	Emissivity = 0.7 300 points in correlation. $L$ = characteristic length. All cylinders 2.8 in. dia.
Acrylic	Ellipsoid 3.0 (minor axis) $G = 0.297 - 1.0$	Air	$\Delta t = 80$	6.9–26	12000– 50000	N/A	$Nu = aRe^b$ $a = 0.32 - 0.22G$ $b = 0.44 + 0.23G$	Ref: Smith et al. (1971)	$G = 1/4 + 3/(8A^2) + 3/(8B^2)$ $A$ = minor length / char. length $B$ = major length / char. length Char. length = $0.5 \infty$ minor axis Use twice char. length to calculate Re.
Acrylic	Spherical 3.0	Air	$t = 24$	2.17 4.04 4.46 5.68	3700– 10000	2.6* 2.5 3.9 3.8	$Nu = 2.58Re^{0.303}Pr^{1/3}$	Ref: Minh et al. (1969)	Random packed. Interstitial velocity used to calculate Re. Bin dimensions: 30 × 18 × 24 in. *Values for top of bin.

<sup>a</sup>Characteristic length is used in Reynolds number and illustrated in the Comments column 10 where appropriate.<sup>b</sup>Characteristic length is given in column 2, free stream velocity is used, unless specified otherwise in the Comments column 10.<sup>c</sup>Nu = Nusselt number, Re = Reynolds number, Gr = Grashoff number, Pr = Prandtl number.

where  $q$  is the heat transfer rate,  $t_s$  is the surface temperature of the food,  $t$  is the surrounding fluid temperature, and  $A$  is the surface area of the food through which the heat transfer occurs.

The surface heat transfer coefficient  $h$  depends on the velocity of the surrounding fluid, product geometry, orientation, surface roughness and packaging, as well as other factors. Therefore, for most applications  $h$  must be determined experimentally. Experimentalists have generally reported their findings as correlations, which give the Nusselt number as a function of the Reynolds number and the Prandtl number.

Experimentally determined values of the surface heat transfer coefficient are given in Table 13. The first two columns of the table describe the product used in the experiment and its shape. Columns 3 through 6 describe the experimental conditions used to determine the surface heat transfer coefficient. Column 7 gives the experimentally determined values of the surface heat transfer coefficient while Column 8 contains the reported Nusselt-Reynolds-Prandtl correlation, if any, and its associated error. Columns 9 and 10 state the source from which the surface heat transfer coefficient data and/or correlation was obtained as well as additional comments.

The following guidelines are important for the use of Table 13:

1. Use a Nusselt-Reynolds-Prandtl correlation or a value of the surface heat transfer coefficient that applies to the Reynolds number called for in the design
2. Avoid extrapolations
3. Use data for the same heat transfer medium, including temperature and temperature difference, which are similar to the design conditions. The proper characteristic length and fluid velocity, either free stream velocity or interstitial velocity, should be used in calculating the Reynolds number and the Nusselt number.

**NOMENCLATURE**

$a$  = parameter in Equation (26):  $a = 3k_c/(2k_c + k_d)$   
 $A$  = surface area  
 $b$  = parameter in Equation (26):  $b = V_d/(V_c + V_d)$   
 $c$  = specific heat  
 $c_a$  = apparent specific heat  
 $c_f$  = specific heat of fully frozen food  
 $c_i$  = specific heat of  $i^{\text{th}}$  food component  
 $c_p$  = constant pressure specific heat  
 $c_u$  = specific heat of unfrozen food  
 $d$  = commodity diameter  
 $D$  = characteristic dimension  
 $E$  = ratio of relative molecular masses of water and solids:  $E = M_w/M_s$   
 $f$  = respiration coefficient  
 $F_l$  = parameter given by Equation (32)  
 $g$  = respiration coefficient  
 $h$  = surface heat transfer coefficient  
 $H$  = enthalpy  
 $H_f$  = enthalpy at initial freezing temperature  
 $H_i$  = enthalpy of the  $i^{\text{th}}$  food component  
 $k$  = thermal conductivity  
 $k_1$  = thermal conductivity of component 1  
 $k_2$  = thermal conductivity of component 2  
 $k_a^r$  = air film mass transfer coefficient (driving force: vapor pressure)  
 $k_a^c$  = air film mass transfer coefficient (driving force: concentration)  
 $k_c$  = thermal conductivity of continuous phase  
 $k_d$  = thermal conductivity of discontinuous phase  
 $k_i$  = thermal conductivity of the  $i^{\text{th}}$  component  
 $k_s$  = skin mass transfer coefficient  
 $k_t$  = transpiration coefficient  
 $k_{\parallel}$  = thermal conductivity parallel to food fibers  
 $k_{\perp}$  = thermal conductivity perpendicular to food fibers  
 $L^2$  = volume fraction of discontinuous phase  
 $L_o$  = latent heat of fusion of water at 32°F = 144 Btu/lb  
 $m$  = mass  
 $\dot{m}$  = transpiration rate  
 $M$  = parameter in Equation (28) =  $L^2(1 - k_d/k_c)$   
 $M_s$  = relative molecular mass of soluble solids  
 $M_w$  = relative molecular mass of water

$n$  = normal surface vector  
 $Nu$  = Nusselt number  
 $N^2$  = volume fraction of discontinuous phase  
 $P$  = parameter in Equation (30) =  $N(1 - k_d/k_c)$   
 $Pr$  = Prandtl number  
 $p_a$  = water vapor pressure in air  
 $p_s$  = water vapor pressure at commodity surface  
 $q$  = heat transfer rate  
 $Q$  = heat transfer  
 $R$  = universal gas constant = 1.986 Btu/lb mol·°R  
 $R_1$  = volume fraction of component 1  
 $Re$  = Reynolds number  
 $R_{H_2O}$  = universal gas constant for water vapor  
 $Sc$  = Schmidt number  
 $Sh$  = Sherwood number  
 $t$  = food temperature, °F  
 $t_f$  = initial freezing temperature of food, °F  
 $t_r$  = reference temperature = -40°F  
 $t_s$  = surface temperature, °F  
 $t$  = ambient temperature, °F  
 $T$  = food temperature, °R  
 $T_f$  = initial freezing point of food item, °R  
 $T_o$  = freezing point of water;  $T_o = 491.7^\circ\text{R}$   
 $T_r$  = reference temperature = 419.7°R (-40°F)  
 $T$  = reduced temperature  
 $u$  = free stream air velocity  
 $V_c$  = volume of continuous phase  
 $V_d$  = volume of discontinuous phase  
 $W$  = rate of heat generation due to respiration, Btu/h-lb  
 $x_1$  = mass fraction of component 1  
 $x_a$  = mass fraction of ash  
 $x_b$  = mass fraction of bound water  
 $x_f$  = mass fraction of fat  
 $x_{fb}$  = mass fraction of fiber  
 $x_i$  = mass fraction of  $i^{\text{th}}$  food component  
 $x_{ice}$  = mass fraction of ice  
 $x_p$  = mass fraction of protein  
 $x_s$  = mass fraction of solids  
 $x_{wo}$  = mass fraction of water in unfrozen food  
 $x_i^v$  = volume fraction  $i^{\text{th}}$  food component  
 $y$  = correlation parameter in Equation (19)  
 $z$  = correlation parameter in Equation (19)  
 $\alpha$  = thermal diffusivity  
 $\delta$  = diffusion coefficient of water vapor in air  
 $\Delta c$  = difference in specific heats of water and ice =  $c_{water} - c_{ice}$   
 $\Delta H$  = enthalpy difference  
 $\Delta T$  = temperature difference  
 $\epsilon$  = porosity  
 $\theta$  = time  
 $\Lambda$  = thermal conductivity ratio =  $k_1/k_2$   
 $\nu$  = kinematic viscosity  
 $\rho$  = density of food item  
 $\rho_1$  = density of component 1  
 $\rho_2$  = density of component 2  
 $\rho_i$  = density of  $i^{\text{th}}$  food component  
 $\sigma$  = parameter given by Equation (33)

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